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NAVAL SHIP RESEARCH AND DEVELOPMENT CENTER BETHESDA --ETC F/G 13/10  
SHIP PROPULSION SHAFTING BEARING REACTION PROGRAMS MGE2 AND MGE--ETC(U)  
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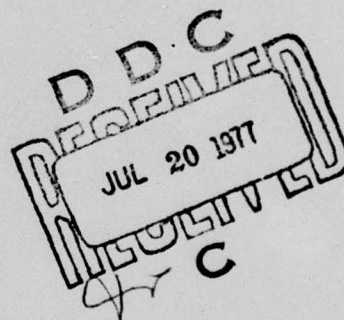
✓ **NAVAL SHIP RESEARCH AND DEVELOPMENT CENTER**

Washington, D.C. 20007



Ship Propulsion Shafting Bearing Reaction  
Programs MGE2 and MGE5 for IBM 7090  
(with notes on Univac LARC)

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August 1967

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Ship Propulsion Shafting Bearing Reaction  
Programs MGE2 and MGE5 for IBM 7090  
(with notes on Univac LARC) .

by

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Sharon E. Good

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# NOTATION

Symbol	FORTTRAN Name	Description
	N	Number of stations.
	NO (I)	Station number of I <sup>th</sup> station.
$x_i$	DISTL (I), A	Length to extreme end from I <sup>th</sup> station in inches.
$d_a$	DIA (I), B	Outer diameter of shaft at I <sup>th</sup> station in inches.
(a) $d_b$	STIFX(I), C	(a) Inner (if hollow) or second (if sleeve) diameter in inches.
(b) $\Sigma EI$ or ST		(b) Stiffness.
(a) $d_c$	WTS(I), D	(a) Third diameter in inches.
(b) $\Sigma A_p$		(b) Weight in lb./in. per unit length.
W	CONWT(I), E	(a) Concentrated Weights in lbs. (negative in sign).  (b) and Bearing reactions (positive in sign).
a	IM (I), I	Outer material at I <sup>th</sup> station (only 1-5 possible).
b	JM (I), J	Inner material at I <sup>th</sup> station (only 1-5 possible).
	IBRG(I), K	Code indicating presence (1) or absence (0) of bearing at station I.
	IS (I)	Code indicating sand (1) or no sand (0) in bore.

Symbol	FORTTRAN Name	Description
E	YMAT, H	Moduli of elasticity in lbs./sq. in. (Young's modulus).
$\rho$	DENMAT, P	Density of shaft materials in lbs./ cu. in.
$l_i = x_{i+1} - x_i$	DIST T(I)	(a) Section length in inches. (b) Stiffness ( $10^{-10}/EI$ )
$M_L = \int_0^L S dL$	BMTAB	Bending moment in $10^{-3}$ inch-lbs.
$\theta_L = \frac{1}{EI} \int_0^L M dL$	THETA	Slope in Radians.
$\delta_L = \int_0^L \theta_L dL$	DEF	Deflection in inches.
$\alpha$	BNFLU	Influence numbers for bearings (lb. per .001-inch rise) and de- flection and slope (for 1-inch rise).
	DIBRG	Section length from support point to extreme end table.
	IBTAB	Bearing index table.
n	IBRS	Number of bearings.
$S_L = \int_0^L W dL$	SFTAB	Shear force in $10^{-3}$ lbs.
	I2 IERROR	Error code in incorrect data preparation.



Symbol	FORTTRAN Name	Description
	TITL2	Case title array for MGE2.
	IXM	Sentinel
	SWAT	
	NS	} Unused options.
	IYM	
R	CANOT	Bearing Reaction in lbs.
	CONOT	
	WBAR	Total Shaft weight including concentrated loads in lbs.
	XBAR	Distance of Center-of-gravity from station no. 1 in inches.
$A_a$	AREA 1	Shaft cross section area, second material.
$A_b$	AREA 2	Shaft cross section area, second material.
$A_c$	AREA 3	Shaft cross section area, sand in bore.
$I_a$	AMI1	Moment of Inertia for first material.
$I_b$	AMI2	Moment of Inertia for second material.
	XBRG	Bearing relocation off straight line.
	TITL5	Case title array for MGE5.

Some storage areas have uses a and b in different sections of the program. The several arrays which have special names in READIN subroutine are listed as second entry in name column.

## ABSTRACT

✓  
MGE2 is a FORTRAN IV program which computes characteristics of the main propulsion shaft of a ship, assuming that all bearing centers are on a straight line. Output from this program consists of the straight-line bearing reactions and the influence numbers for each support point. These influence numbers indicate the changes in supporting reactions produced by the raising or lowering of a particular bearing. The program also calculates the shear, bending moment, slope, and deflection values, and the weight and stiffness factors for stations designated along the shaft.

MGE5 is a program similar to MGE2. It is a design tool for determining the effects of bearing centers at any given elevation relative to the straight line. MGE5 is often used after MGE2 to determine the reactions of realigned bearings. Output from MGE5 includes bearing reactions at each support point and shear, bending moment, and slope and deflections values at designated stations. ↗

## ADMINISTRATIVE INFORMATION

The work reported herein was authorized under job number 1-890-202-01.



## INTRODUCTION

**MGE2** gives the characteristics of a shaft with all bearings, or support points, on a straight line. Output includes shear, bending moment, slope, and deflection as well as weight and stiffness factors at designated stations along the shaft. A table of influence numbers is listed for each bearing. These influence numbers indicate the changes in supporting reactions caused by the raising or lowering of a particular bearing.

**MGE5** calculates shear, moment, slope, and deflection at various stations and bearing reactions, with bearing centers set in any given elevation relative to a straight line.

The programs were coded in **FORTRAN IV** with the exception of **MAP** double precision routines in the 7090 matrix inversion portion. Decks or further information are available from Code 830, Naval Ship Research and Development Center (NSRDC), Washington, D. C. 20007.

These programs have also been run on **LARC** and 7090 in **FORTRAN II**.

## METHOD OF CALCULATION

(Taken from the "Calculation of Ship Propulsion Shafting Bearing Reactions on an IBM 650 Computer" written by Edward T. Antkowiak)

"Although the texts on indeterminate structures illustrate various devices for handling continuous beams on multiple supports, such as Hardy Cross or Relaxation Method, Three Moment Equations, etc., the large memory capacity and speed of a digital computer permits a more 'classical' approach. This approach is based on a direct evaluation of the relationship of the beam load ( $w$ ) to the deflection ( $\delta$ ).

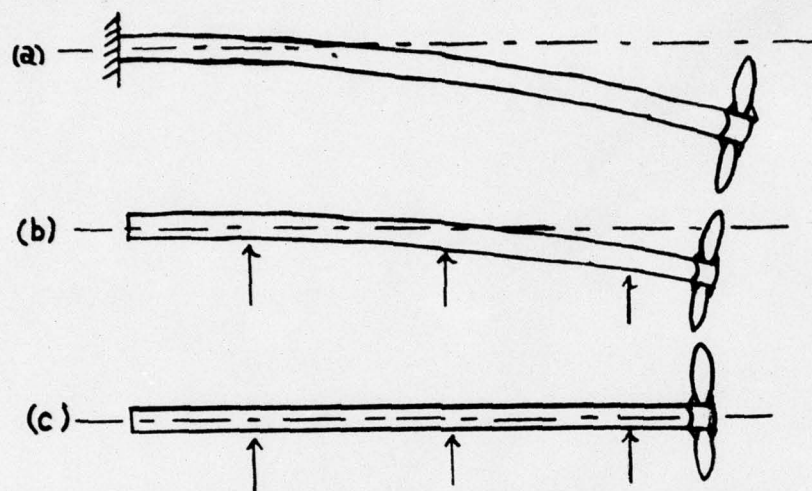
$$EI \frac{d^4 \delta}{dx^4} = W$$

"Therefore, successive integrations of the load-stiffness diagram will yield shear, moment, slope and deflection. However, in order to obtain zero deflection at each support, the correct reactions would have to be included in the load diagram prior to the integration. In the shafting problem, the reactions at each support are the unknowns.

"If the reactions are not included in the load diagram and it is assumed that the beam is held firmly at one end, the successive integrations will result in a deflection diagram similar to that shown in Figure 1 (a). Applying estimated reactions whose magnitudes are proportional to the deflection will yield a diagram with a smaller deflection, as shown in Figure 1 (b). Further approximations and successive integrations will converge to a zero deflection at the



supports, as shown in Figure 1 (c). At this point, the correct reaction has been applied.



**Figure 1 - Convergence of Shaft Deflection Curve to a Straight Line by Adding Support Reactions**

"In order to apply this principle to practical use, some method of obtaining reaction estimates had to be devised. The method used is to determine the amount of reaction change produced by raising or lowering a bearing support a unit amount. This is also one of the final answers to our problem. These influence numbers are obtained by assuming the shaft has no weight and that a unit reaction is applied to one bearing. Successive integrations will then yield resulting deflections at all other bearing locations. By applying this unit reaction to each support in turn, a family of deflections will be obtained which can be substituted into a set

of equations (two more equations than there are number of support points), expressing the relationship of reactions and deflections. Solution of these equations will yield the 'influence numbers' necessary to the final solution of straight line reactions.

"Multiplying the influence numbers by the deflections obtained from integration of the unsupported, weighted (real) shaft, and summing the reaction changes for each bearing, the final straight line reactions will result. Applying this total reaction for each bearing to the load diagram and repeating the integration process, the deflection at each support will be zero, thus proving that the correct reaction has been applied. If the deflection is not zero, the entire process can be repeated until the bearing deflection becomes trivial."



## THEORY

Figure 2 shows a sample section of shaft with nomenclature as in the Notation. The programs compute moment of inertia and weight per unit length as follows:

Outer area

$$A_a = \pi/4 (d_a^2 - d_b^2)$$

Inner area

$$A_b = \pi/4 (d_b^2 - d_c^2)$$

Innermost area

$$A_c = \pi/4 d_c^2$$

Inertia of outer part

$$I_a = \pi/64 (d_a^4 - d_b^4)$$

Inertia of inner part

$$I_b = \pi/64 (d_b^4 - d_c^4)$$

Weight per unit length

$$A_a \rho_a + A_b \rho_b + A_c \rho_c - (A_a + A_b + A_c) \rho_d$$

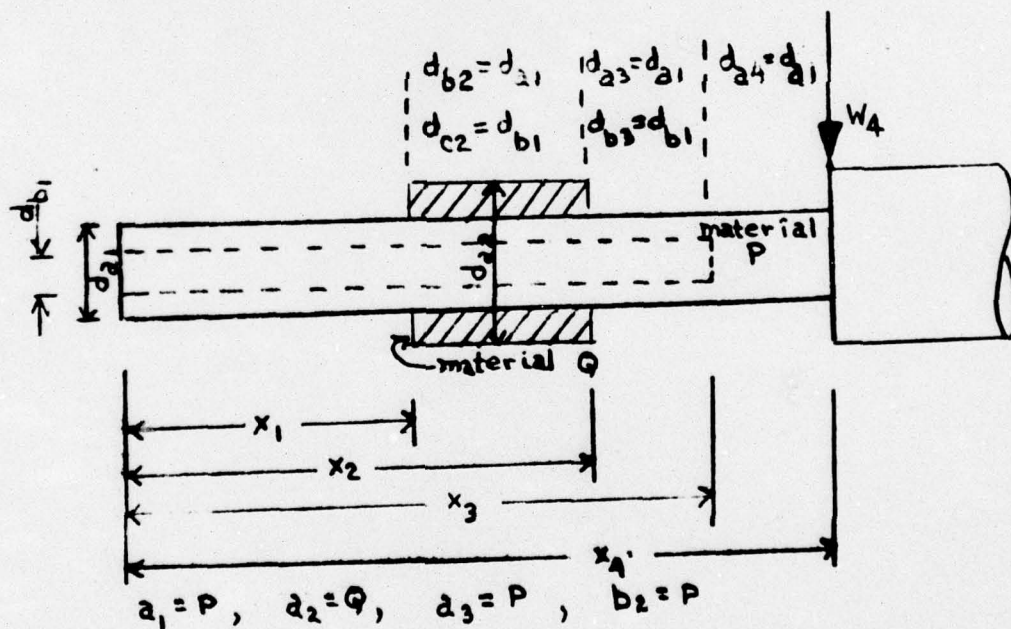


Figure 2 - Section of Shaft with Computational Inputs Labelled

where the first term (Material a ) must be present in all cases; the second term (b) will be present for two materials; the third (c) is present only if the bore is filled with sand; and the fourth (d), which represents the upthrust of water, is present only if the shaft is wholly or partly immersed in water.

Consider a shaft of no weight but with the same stiffness as the real weighted shaft. If such a weightless shaft were on "straight line" bearings, there would be no reaction; however, if one of the bearings should be raised by 1 mil, forces would occur at each bearing.

These forces are the "influence numbers" which form an  $n \times n$  matrix where  $n$  is the number of bearings. The element in the  $i^{\text{th}}$  column and  $j^{\text{th}}$  row gives the force on Bearing  $i$  for a deflection of 1 mil at Bearing  $j$ .

Consider the weightless shaft acting as a cantilever as shown in (a) of Figure 3. When a unit force is applied at B, Section AB will be

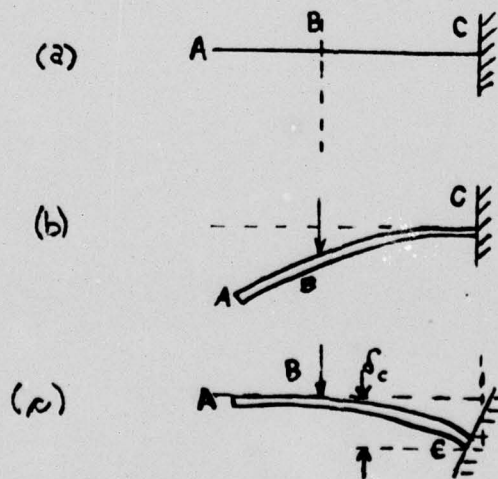


Figure 3 - Force Applied to a Weightless Cantilevered Beam

straight, but inclined at an angle to the horizontal (b). There is an advantage to assuming that Section AB remains horizontal with the wall moved (c), using AB as the reference axis.

Now consider the shear force, bending moment, slope, and deflection diagrams. According to the theory of beam deflection, these diagrams are related to one another by integration (see Figure 4).

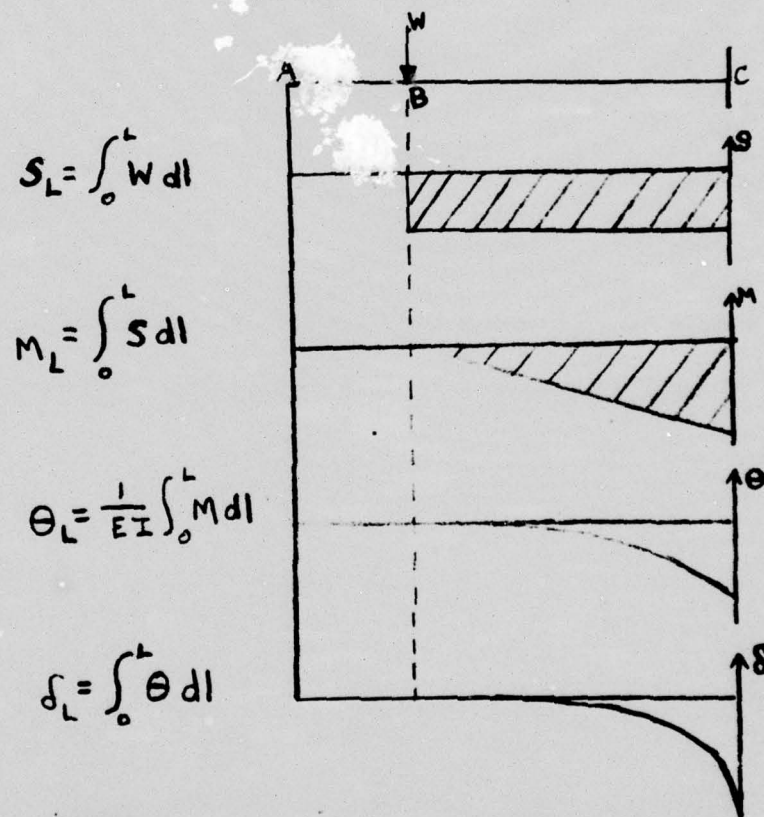


Figure 4 - Successive Integrations of a Load Stiffness Diagram

The result of a series of such integrations is summarized in tabular form by Table 1. Thus  $d_{24}$  is the deflection at Station 4 for a force of unity applied at Station 2.



TABLE I

Table of Deflections Resulting from Applying  
Individual Unit Reactions

Force Applied at Station Number:						Deflection at Station Number:					
1	2	3	4	5	6	1	2	3	4	5	6
1							$d_{12}$	$d_{13}$	$d_{14}$	$d_{15}$	$d_{16}$
	1							$d_{23}$	$d_{24}$	$d_{25}$	$d_{26}$
		1							$d_{34}$	$d_{35}$	$d_{36}$
			1							$d_{45}$	$d_{46}$
				1							$d_{56}$
					1						



If the beam Section AB is not considered to be horizontal or at zero slope, these deflections must be corrected as follows:

At A: add  $\Delta_o$

At B: add  $\Delta_o + \theta_o x_1$

At C: add  $\Delta_o + \theta_o x_2$  (see Figure 5).

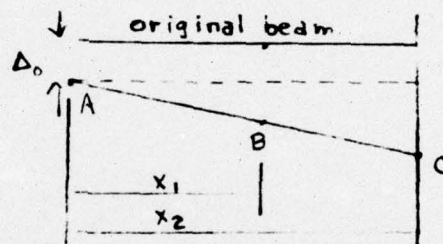


Figure 5 - Beam (Shaft) Displaced from Horizontal Reference Line

When unit reactions  $R_1, R_2, \dots, R_n$  occur at support points 1, 2,  $\dots$  n along the weightless shaft, the following equations apply:

$$\delta_1 = \Delta_o + \theta_o x_1$$

$$\delta_2 = \Delta_o + \theta_o x_2 + d_{12} R_1$$

$$\delta_n = \Delta_o + \theta_o x_n + d_{1n} R_1 + d_{2n} R_2 + \dots + d_{(n-1)n} R_{(n-1)}$$

Two additional equations are required to solve this group; they may be found by considering the beam end C in Figure 5 as unfixed when it is

supported by reactions along its length. When acting as a multiply supported beam, this free end has no shear or moment, such that

$$0 = R_1 + R_2 + \dots + R_n$$

$$0 = x_1 R_1 + x_2 R_2 + \dots + x_n R_n$$

All these equations can therefore be put into a  $n+2$  equation square matrix form

$$\begin{bmatrix} \delta_1 \\ \delta_2 \\ \delta_3 \\ . \\ . \\ . \\ \delta_n \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 & X_1 & 0 & 0 & 0 & \dots \\ 1 & X_2 & d_{12} & 0 & 0 & \dots \\ 1 & X_3 & d_{13} & d_{23} & 0 & \dots \\ . & . & . & . & . & . \\ . & . & . & . & . & . \\ . & . & . & . & . & . \\ 1 & X_n & d_{1n} & d_{2n} & d_{3n} & \dots \\ 0 & 0 & 1 & 1 & 1 & \dots \\ 0 & 0 & X_1 & X_2 & X_3 & \dots \end{bmatrix} \times \begin{bmatrix} \Delta_0 \\ \theta_0 \\ R_1 \\ . \\ . \\ . \\ . \\ . \\ R_n \end{bmatrix}$$

representing the deflections for a given reaction. Inversion of this matrix gives the reactions for a given deflection, the reaction influence numbers. The columns which give deflection and slope condition now give slope and deflection influence numbers (i. e. , the end slope and

the deflection for a given deflection at an intermediate point). Thus  $\alpha_{32}$  represents the reaction at Support 3 for a theoretical unit deflection at Bearing 2.

Assuming the initial slope and deflection are zero and that reactions at support points are zero (shaft cantilevered at one end), the end shear ( $V_1$ ) and end moment ( $M_1$ ) of the weighted shaft are calculated. These results are used to modify the first ( $R_1$ ) and last ( $R_n$ ) reactions, so that  $V_1$  and  $M_1$  then approach zero.

Consider the actual shaft with only two external bearings, held at the end to ensure no initial slope and deflection (see Figure 6), with total shaft weight  $W$ , total moment from the other end  $M$ , and total length  $L$ . (The convention assumed is that all downward forces are negative.)

$$\text{Then: } R_a + R_b = -W$$

$$(L-x_1) R_a + (L-x_n) R_b = -M$$

from which  $R_a$  and  $R_b$  are found. The new moments, slopes, and deflections can be found by considering the real weight shaft with concentrated loads.

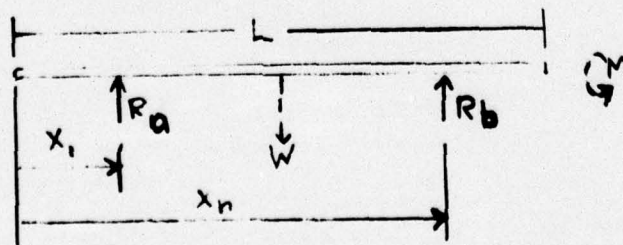


Figure 6 - Real Weighted Shaft with Only Two Bearings Present



The above discussion presents the solution to the two-bearing problem. Then, by using the influence numbers, the effect on the reactions when all the bearings are moved to the correct position can be found;  $\Delta_0$  and  $\theta_0$  are modified at this time.

The actual answers from the inversion will not be exact, but repeated entry into the deflection integration routines will give corrected values of the deflection for all bearings. Several of these weighted integrations may be required to obtain results within the required margin.

## MGE2 - STRAIGHT-LINE BEARINGS

### PROGRAM DESCRIPTION

To calculate the characteristics of a shaft with all supports on a straight line as outlined in "Method of Calculation," the shafting system must be divided into a number of stations, subject to the following restrictions:

1. Total number of stations must not exceed 400.
2. Total number of supports must not exceed 22.
3. Each change in cross-section diameter, each bearing location, each concentrated load, and the beginning of each immersion requires a new station.
4. Although the length of each station is arbitrary, there should be enough of these stations to provide sufficient abscissa points for plotting shear, moment, slope, and deflection diagrams, if desired.
5. All stations (except the last) must have nonzero diameter and material. The last data card is not considered a section; it serves to specify the total length of the shafting system.
6. Bearing may not occur at the first or at the last station.
7. Concentrated loads should not appear at bearing locations since calculated bearing-reaction values will overwrite the concentrated loads. Add an additional shaft section with a 0.100-inch, or even a 0.0001-inch, separation.



The program is written in a general manner and provides for the following variables:

1. Material of shaft
2. Shaft in air or water
3. Shaft solid or hollow
4. Sand in bore of hollow shaft

The specific moduli and densities in the program are:

Code	Material	Density (lb/cu in.)	Modulus (lb/sq in.)
1	Steel	-.28355	$30 \times 10^6$
2	Bronze	-.31399	$15 \times 10^6$
6	Sand	-.0636	
7	Salt water	-.03705	

If materials used in a specific shaft have constants quite different from the above, additional values may be added.

Slight changes in diameter may be ignored when the effect on weight and stiffness of the shaft is negligible. The average diameter of the propeller taper is used.

Loads acting downward will be negative. In most cases, reactions will be positive. However, in some instances where several bearings are close together, one bearing may indicate a negative reaction for the straight-line condition.

The weight of the propeller is applied as a concentrated load at its center of gravity, if known; otherwise, the weight is considered to



act at the middle of the tapered section. The dry weight of an immersed propeller may be reduced to take into account the buoyant effect of water by using the relationship

$$W \text{ (water)} = W \text{ (air)} * \frac{D_p - D_w}{D_p}$$

where  $D_p$  is the density of the propeller material and  $D_w$  is the density of the water.

Bearing reactions are assumed to act at points in the middle of the fore and aft ends of the bearings. However, in the case of a relatively long bearing such as a stern tube, it may be assumed that the load is concentrated one shaft diameter forward of the aft end of the bearing. For a more detailed study, support points at several positions along a bearing may be assumed.

The program gives the magnitude of all bearing reactions, assuming all bearings on a straight line. It prints slope and deflection influence numbers, which represent the amount of change in all bearing loads resulting from raising a particular bearing 0.001 in. from the straight line. Values of shear, moment, slope, deflection, weight (in pounds per inches), and stiffness (in terms of  $\frac{1}{EI}$ ) are given for each station. The total weight of the shaft and the location of the center of gravity are also printed.

The criteria for determining zero deflection at a bearing and the absence of shear force or moment at the free end are listed below:

1. Deflection at a bearing no greater than 0.001 in.
2. Shear force at free end less than 10 lb.
3. Bending moment at free end less than 100 in.-lb.
4. A maximum of four iterations on the deflection check.
5. A maximum of four iterations on the shear and moment checks.

The following error printouts occur after unrecoverable errors have been detected. The program then transfers to next data case.

The printout TOO MANY ITERATIONS DEFL XXXX MOMENT XXXX occurs when four iterations through DEFLN and BEAM have failed to meet terminal deflection, bending moment, and shear force criteria. The current results are then accepted.

The printout STATION DISTANCE ERROR occurs when stations are not input in ascending order of distance from Station 1. Case is terminated.

The printout SINGULAR INFLUENCE NUMBERS occurs if matrix is singular. Since it is indicative of incompatible data, case is terminated.

## OPERATING INSTRUCTIONS

1. The program run with 7090 IBSYS Version 13 includes the following cards:

<b>\$JOB</b>	
<b>\$EXECUTE</b>	<b>IBJOB</b>
<b>\$IBJOB</b>	<b>FIOCS</b>

decks	<b>MGE2</b>
	<b>RED2</b>
	<b>BEAM</b>
	<b>DEFL</b>
	<b>INOUE</b>
	<b>INFN</b>
	<b>AM MAT2</b>
	<b>AM DPAF</b>

### **\$DATA**

**MGE2** heading card for input case 1  
One card per station for input case 1  
One card for each constant change (omit if no material  
constant changes)  
Sentinel card with punch in column 2  
Additional cases of data, if called for by sentinel

.

.

.

Final sentinel has 9- or 7-punch in column 2

$\frac{7}{8}$  **END OF FILE**

2. Output of five or more pages per case is written on **SYSDU1** for program control printing.

At NSRDC, when compiled with plot option, control cards

<b>\$ATTACH</b>	<b>B9</b>
<b>\$AS</b>	<b>SYSLB4</b>

are inserted before **\$ EXECUTE** card, and plots for **SC 4020** may be



prepared on SYSLB4. Deck GRAP must also be included before \$DATA card.

3. Total time for IBSYS compile, load, and execute of six varied cases was 1.8 min. Since the load time for retrieval of binary program deck from master instruction reel with \$IEDIT is 1 min, it is obviously advantageous to run multiple cases.

4. No sense switches, sense lights, or scratch files are used by the program. Memory requirement (including I/O subroutines) 19,400. For smaller computer, dimensions could be revised.

5. The program run on LARC includes:

Data cards for Program MGE2, followed by six cards with END OF TAPE punched in columns 1-12, are converted to tape and ready for mounting on Unit 11.

Object code tape containing instructions for routine

MGE2  
READ2  
BEAM  
DEFL  
INOU  
INFN  
AM MAT2L

is mounted on Unit 13.

Output is written on Tape 20 for 1/1 LSC loop printing.

## SC 4020 PLOTS

An option for SC 4020 graphic output may be used at NSRDC on 7090 or LARC. Card MGE2 0164 (or MGE5 0119) is changed from  
981 CONTINUE to 981 CALL GRAPH

The graph routine is listed in Appendix A.

The two sets of plots made for each case are moment and deflection versus station distance. If the total number of stations is less than 99, one frame is produced for each graph. For larger numbers of stations, a fixed station distance scale of 450 ft/frame results in 2 to 21 frames for each graph.

The ordinate versus abscissa is plotted as a continuous line with bearing stations further identified by X. See Appendix A for sample output.

## SHAFT ARRANGEMENT

Figure 7 shows a typical line shaft dimensioned for preparation of input data. The sketch should be made to some appropriate scale, using information from arrangement, assembly, and detailed drawings of low speed gear and shaft. The relationship of the components can then be readily observed.

1. The total number of stations must not exceed 400 and the total number of support points must not exceed 22.

2. Station 1 is the forward end of the shaft and all other stations are located in terms of their distance from Station 1. A station must be initiated at each support point, at each concentrated load, and at each significant change in cross-section diameter. Concentrated loads should not appear at bearing locations; an additional station with 0.001- or 0.0001-in. separation may be used (see note at end of paragraph). To reduce the number of stations, slight changes in diameters may be ignored or combined when their effect on the weight and stiffness of the shaft is negligible. Thus, in Figure 7, since the journal sections were only 1/4 in. wider than the shaft, they were considered to be the same diameter as the shaft. Also the average diameter of the tapered propeller section was used. Note that, if desired, the additional weight of journal sections may be compensated for without increasing the number of stations by adding the weight as concentrated load at the center of the



bearing, but such a load would not be included in the bearing reactions given as output. All concentrated weights, however, are included in the total weight of the shaft.

3. Where the thrust collar is forward of the low speed gear and not integral, its weight is treated as a concentrated load, since it does not add significantly to the stiffness of the system. In Figure 7, the thrust bearing is aft of the low speed gear and the thrust collar is integral with the shaft; therefore, it is treated as part of the shaft.

4. a. Since the gear is not a solid section (rim, webs, etc.), an equivalent outside diameter must be used to obtain its proper lateral stiffness. The outside diameter of the hub section may be used as the equivalent outside diameter.

b. The difference between the total weight of the actual low speed gear and shaft assembly and the calculated weight of the equivalent assembly is applied as a concentrated load on this section so that the total weight will be correct.

c. In Figure 7, this difference is applied as one concentrated load at the centerline of the gear, midway between fore and aft bearings. Present practice is to divide the concentrated load by the number of webs, and to apply these equal loads at the points where the webs meet the hub. In most cases, either method may be used.

5. Bearing reactions are assumed to act at points midway between the fore and aft ends of each bearing. In the case of long bearings (such as a stern tube bearing), it may be assumed that the load is concentrated one shaft diameter forward of the aft end of the bearing. For a more exact detailed study, support points at several positions along a bearing may be assumed.

6. If the shaft is to be studied with the ship waterborne, a note should be made on the sketch (Figure 7) to indicate what portion of the shaft is to be immersed. A station must be initiated at the beginning of the immersion.

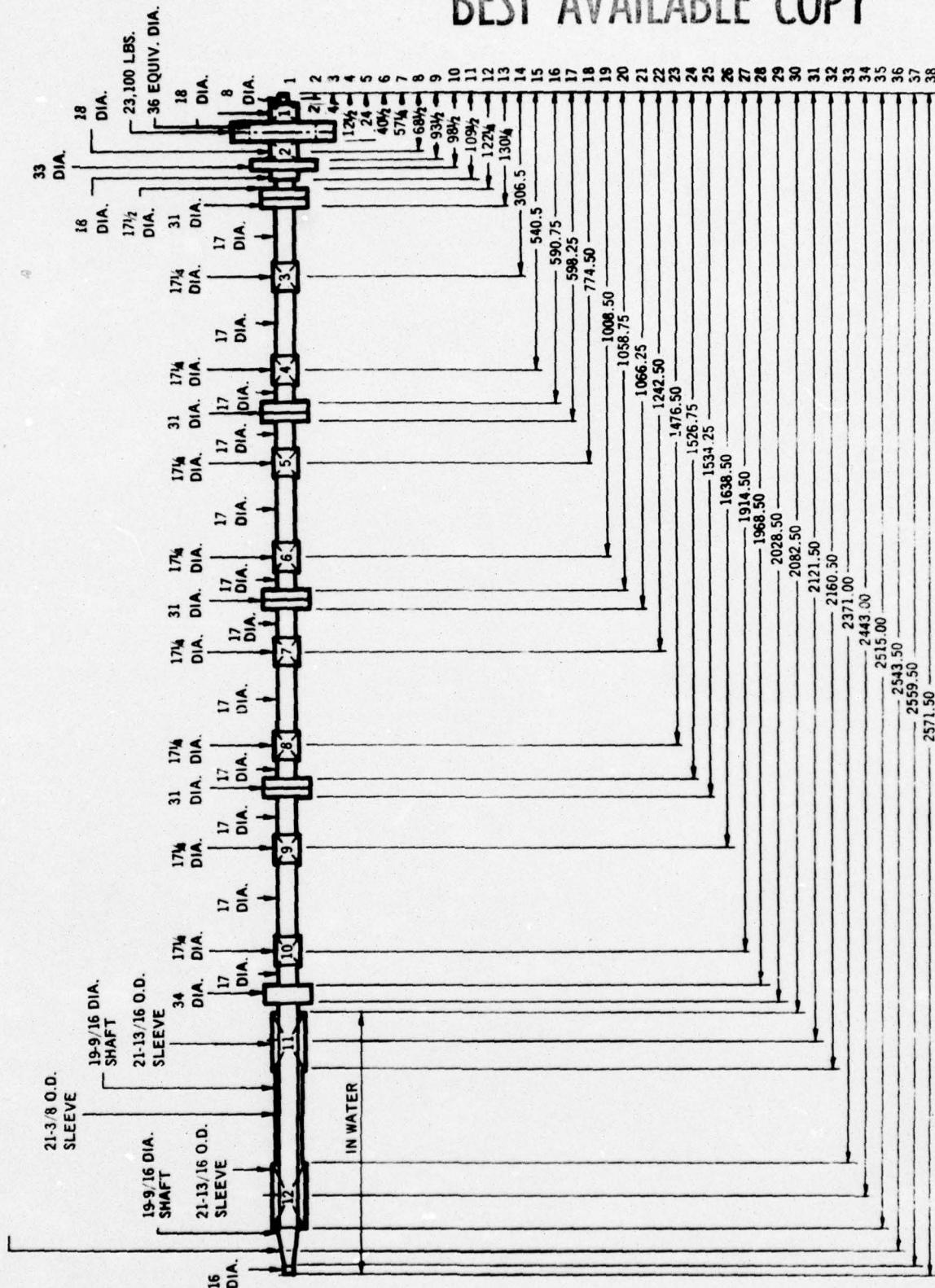
7. The weight of the propeller is applied as a concentrated load at its center of gravity, if known; otherwise, the weight is considered to act at the middle of the tapered section. The dry weight of an immersed propeller should be reduced to take into account the buoyancy effect of salt water by the relationship

$$\text{Weight (water)} = \text{Weight (air)} \times \frac{(\text{Density (prop)} - \text{Density (water)})}{\text{Density (prop)}}$$

For bronze with a density of 0.31399 lb/cu in. and salt water with a density of 0.03705 lb/cu in., the multiplicative factor would be 0.882.



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TOTAL WT. OF L.S. GEAR & SHAFT - 40.500 LBS. SHAFT ONLY - 11.05 LBS. ESTIMATED EQUIV. DIA. OF HUB FOR LATERAL STIFFNESS - 36 O.D.

Figure 7 – Shafting Arrangement Dimensioned for Computer Program



## DATA PREPARATION

1. MGE2 Title Card: Columns 1-72 alphanumeric information to identify the case.
2. One card for each station (maximum of 400) in accordance with **FORMAT (I3, 5F12.4, 2I2, 2I1).**

Column No.	Explanation
------------	-------------

1-3	Station number right justified ( $\Delta\Delta 1, \Delta\Delta 2, \dots, 105, 106$ , etc.). Last station must have 9 in column 1 as sentinel.
*4-15	Distance of beginning of station from Station 1, in inches.
*16-27	Outer diameters, in inches.
*28-39	Second diameter, in inches. Inner diameters of bushing or sleeve if used, or diameters or bore if hollow shaft.
*40-51	Third diameter, in inches. Diameter of bore in a hollow shaft which also has bushing or sleeve.
*52-63	Concentrated weight (if present) minus values for downward weight.
64 blank	
65	**Material of outer diameters { 1, if steel 2, if bronze
66 blank	
67	**Material of inner diameter { 1, if steel 2, if bronze
68	Bearing position - blank, if no support; 1, if bearing present.
69	1, if shaft in water; blank, if in air.
70	1, if sand bore; blank, if no sand.

\* The above numbers may be punched anywhere in field, and the decimal point must be punched.

\*\* If material is other than steel or bronze, new constants for density and modulus of elasticity must be given.

3. One card for each new material or change of density and modulus of elasticity using FORMAT (2I2, 2F12, 2). (Omit if no material constant changes.)

Column No.	Explanation
------------	-------------

2	Code for action to be taken: 1 - new density only 2 - new modulus only 3 - new density and modulus 4 - set to punch influence numbers (not activated in current program)
4	Code for material: 1 - steel 2 - bronze 6 - sand 7 - water 3, 4, 5 - for new materials
5-16	New density if 1 or 3 in column 2 New modulus if 2 in column 2
17-28	New modulus if 3 in column 2

4. End of Case sentinel card (I2).

Column 2	Explanation
----------	-------------

0 or blank	End last case, no graphs.
7	End last case after graphing
8	Graph, then more cases follow.
9	More cases follow, no graphs.
5, 6	Same as 0.



## MEG5 - BEARINGS RAISED OR LOWERED

### PROGRAM DESCRIPTION

The table of influence numbers obtained from MGE2 enables the calculation of reactions when certain bearings are moved vertically off the straight line. However, MGE5 must be used to find the shear force, bending moment, slope, and deflection at each station caused by raising or lowering certain bearings.

When a study of shaft characteristics from MGE2 suggests that a better alignment could be achieved by raising or lowering certain bearings, MGE5 should be run to determine whether the repositioning imposes excessive shear forces or bending moments on the shaft.

The same general computational procedure is used for both MGE5 and MGE2. However, since the influence numbers and weight and stiffness factors of the shaft system are not affected by changing the elevation of bearings, the output of this MGE5 program does not list these factors. It gives instead a single page of shear, moment, slope, deflection, and bearing reactions.

Restrictions on input are the same as those for MGE2.



## OPERATING INSTRUCTIONS

1. The program run with 7090 IBSYS Version 13 includes:

**\$JOB**  
**\$EXECUTE**                      **IBJOB**  
**\$IBJOB**                              **FIOCS**

                decks        **MGE5**  
                                **RED5**  
                                Beam and rest of decks same as **MGE2**

### **\$DATA**

**MGE5** heading card for input case 1  
One to give bearing change cards  
**MGE2** heading card for input case 1  
One card per station for input case 1  
One card for each constant change (omit if no material  
                                constant changes)  
Sentinel card with column 2 punched  
Additional sets of input data if called for by sentinel  
.  
.  
.  
Final sentinel has 9-or 7-punch in column 2.  
**END OF FILE**

2. Output of one page per case is written on **SYSOU1** for program control printing. Plot option is as in **MGE2**.
3. Execution time is similar to **MGE2**.
4. The program run on **LARC** includes:

                Data cards for Program **MGE5**, followed by six cards with  
**END OF TAPE** punched in columns 1-12, are converted to tape for  
mounting on Unit 11.

Object code tape containing instructions for routines

MGE5  
READ5  
BEAM  
DEFL  
INOI  
INFN  
AM MAT2L

is mounted on Unit 13.

Output is written on Tape 20 for 1/1 LSC loop printing.

## DATA PREPARATION

1. MGE5 Title Card: Columns 1-72 alphametic information to identify how case differs from similar MGE2 run.
2. One to five bearing change cards using FORMAT (I1, 5F11.8).

Column No.	Explanation
1	Blank or 0, if not last card; 9, if last change card.
2-12	Relocation of bearing 1 from straight line.
13-23	Relocation of bearing 2 from straight line.
24-34	Relocation of bearing 3 from straight line.
35-45	Relocation of bearing 4 from straight line.
46-56	Relocation of bearing 5 from straight line.

Next card would contain relocation for next five bearings. Values are given in inches; location of bearing may be punched anywhere in field and the decimal point must be punched.

Plus value is bearing above the line; minus value is below.

3. A complete set of MGE2 input cards, including case sentinel.



## ACKNOWLEDGMENTS

These programs are adaptations of shafting systems programs written originally for IBM 650 by Mr. Edward Antkowiak of the Boston Naval Shipyard; his assistance in preparing this version is appreciated. Much of the coding of an expanded shafting program for IBM 704, done by Mr. Edgar H. Sibley and others at the General Electric Lynn Digital Computer Section, is included within this program. Mr. Ralph E. Wolfe of the Boston Naval Shipyard contributed greatly to the theoretical approach to this calculation and originated the concept of obtaining the influence numbers by integration of a "weightless" shaft. Mr. Frank Zaher of Naval Ship Systems Command and Mr. Edward Ryan, formerly of New York Naval Shipyard, made suggestions which have been incorporated in the final program.

Other versions of the shafting program, written at Boston Naval Shipyard, are also available for IBM 1620 and Burroughs Datatron 205.

# APPENDIX A

## MGE2 - PROGRAM LISTING

```

$IBFTC MGE2 DECK
C SHAFTING BEARING REACTIONS MGE2
C S. GOOD DAVID TAYLOR MODEL BASIN MAY,1963
C STRAIGHT LINE BEARING REACTIONS
C IDENTIFY MATERIALS ...STEEL...1
C BRONZE...2
C SAND...6
C WATER...7
C
C DIMENSION DISTL(401),DIA(401),STIFX(401),WTS(401),CONWT(401),
1IM(401),JM(401),IBRG(401),IWATR(401),IS(401),YMAT(7),DENMAT(7),
2DISTT(401),BMTAB(1620),THETA(802),DEF(401),BNFLU(25,25),DIBRG(25)
3,IBTAB(25),SFTAB(1620),TITL2(12),NO(400)
COMMON N,NO,DISTL,DIA,STIFX,WTS,CONWT,IM,JM,IBRG,
1 IWATR,IS,YMAT,DENMAT,DISTT,BMTAB,THETA,DEF,BNFLU,DIBRG,IBTAB,
2 IBRS,SFTAB,I2,IERROR, TITL2,IXM
DIMENSION CANOT(401),CONOT(25)
DIMENSION NS(50)
COMMON SWAT,NS,IYM
1 FORMAT(12A6)
24 FORMAT( /14X,
1 (LB. PER 0.001 INCH RISE OF BEARING) //)
200 FORMAT(I4,11F10.1)
203 FORMAT(///7H BRG. /115H NO. 1 2 3 4 5 6 7 8 9 10
1 4 5 6 7 8 9 10
2 11 //)
205 FORMAT(///7H BRG. /115H NO. 12 13 14 15 16 17 18 19 20 21
115 16 17 18 19 20 21
2 22 //)
20 FORMAT(115H STATION SECTION FIRST SECOND
1THIRD CONCENTRATED MATERIALS BEARING IN WITH /
2 115H NO. DISTANCE DIAMETER DIAMETER
1IAMETER WEIGHT (INCH) POSITION WATER SAND /
4 115H (INCH) (INCH) (INCH) //)
1(INCH) (LB.) DEFLECTION AND SLOPE INFLUENCE NUMBERS
1000 FORMAT(111H0 IN STATION 1 (FOR ONE INCH OF RISE OF BEARING) //95H
IN STATION 1 (FOR ONE INCH OF RISE OF BEARING) //95H
MGE20001
MGE20002
MGE20003
MGE20004
MGE20005
MGE20006
MGE20007
MGE20008
MGE20009
MGE20010
MGE20011
MGE20012
MGE20013
MGE20014
MGE20015
MGE20016
MGE20017
MGE20018
MGE20019
MGE20020
MGE20021
MGE20022
MGE20023
MGE20024
MGE20025
MGE20026
MGE20027
MGE20028
MGE20029
MGE20030
MGE20031
MGE20032
MGE20033
MGE20034
OMGE20035
MGE20036

```







```

2003 BMTAB(ISET)=C.0
      SFTAB(ISET)=C.0
      DO 2004 ISET=1,401
2004   CANOT(ISET)=0.0
      NIB=1
      IERROR = 1
      READ (5,1) TITL2
      WRITE (6,1036) TITL2
      WRITE (6,20)
      CALL READIN
      IF(IERROR-1) 57,57,560
57    CALL INFNOS
62    WRITE(6,1030) TITL2
      CALL INOUT
      WRITE(6,1000)
      WRITE(6,1010)(NO(J),(BNFLU(JA,J),JA=24,25),J=1,IBRS)
      IF(IERROR-1) 65,65,560
65    CALL DEFLN
      I2=4*N+4
      WBAR=SFTAB(I2)
      XBAR= DISTL(N+1) -BMTAB(I2)/SFTAB(I2)
      CALL BEAM
      CALL DEFLN
      K=N+1
230   WRITE(6,1030) TITL2
      WRITE(6,24)
      KTEST = 0
      KTES2=0
210   DO 300 I1=1,IBRS
      IBSR=IBTAB(I1)
      DO 250 I3=1,IBRS
      IASR=IBTAB(I3)
250   CONWT(IBSR)=DEF(IASR)*BNFLU(I1,I3)*(-1000.0) +CONWT(IBSR)
      THETA(1)= THETA(1)-(DEF(IBSR)*BNFLU(25,I1) )
300   DEF(1)=DEF(1) - ( DEF(IBSR)* BNFLU(24,I1) )
979   CALL DEFLN

```

MGE20109  
MGE20110  
MGE20111  
MGE20112  
MGE20113  
MGE20114  
MGE20115  
MGE20116  
MGE20117  
MGE20118  
MGE20119  
MGE20120  
MGE20121  
MGE20122  
MGE20123  
MGE20124  
MGE20125  
MGE20126  
MGE20127  
MGE20128  
MGE20129  
MGE20130  
MGE20131  
MGE20132  
MGE20133  
MGE20134  
MGE20135  
MGE20136  
MGE20137  
MGE20138  
MGE20139  
MGE20140  
MGE20141  
MGE20142  
MGE20143  
MGE20144

```

DO 400 I=1,IBRS
J=IBTAB(I)
IF (ABS (DEF(J))- .001)400,400,445
400 CONTINUE
IF (KTEST-4) 410, 450, 450
410 IF (ABS(BMTAB(I2))-100.)420,222,222
420 IF (ABS(SFTAB(I2))-10.)1500,222,222
222 KTEST = KTEST +1
CALL BEAM
GO TO 979
445 KTES2=KTES2+1
IF (KTES2-4) 210, 450, 450
450 WRITE(6,451) KTES2,KTEST
451 FORMAT(27H000 MANY ITERATIONS - DEFL I4, 9H MOMENT I4)
500 DO 515 I=1,K
DISTT(I)= 0.0
IF (STIFX(I))515,515,514
514 DISTT(I)=1.E12/STIFX(I)
515 CONTINUE
800 DO 825 I=1,IBRS
J=IBTAB(I)
CONOT(I)=CONWT(J)
825 CANOT(J)=CONCT(I)
IF (IBRS-11) 350,350,351
350 K2 =IBRS
GO TO 310
351 K2 = 11
310 CONTINUE
320 WRITE(6,203)
DO 322 J=1,IBRS
322 WRITE(6,200)NO(J), (BNFLU(I,J), I=1,K2)
WRITE (6,1035)
WRITE (6,1037) (CONOT(I),I=1,K2)
352 IF (IBRS-11)517,517,357
357 WRITE (6,205)
DO 358 J=1,IBRS

```



MGE20145  
 MGE20146  
 MGE20147  
 MGE20148  
 MGE20149  
 MGE20150  
 MGE20151  
 MGE20152  
 MGE20153  
 MGE20154  
 MGE20155  
 MGE20156  
 MGE20157  
 MGE20158  
 MGE20159  
 MGE20160  
 MGE20161  
 MGE20162  
 MGE20163  
 MGE20164  
 MGE20165  
 MGE20166  
 MGE20167  
 MGE20168  
 MGE20169

```

358 WRITE (6,200) NO(J),(BNFLU(I,J),I=12,IBRS)
      WRITE (6,1035)
      WRITE(6,1037) (CONOT(I),I=12,IBRS)
517  CONTINUE
540 WRITE(6,1030) TITL2
      WRITE (6,1031)
      DO 545 I=1,K
        IB = I+1
        IA = IB+IB
545 WRITE(6,1050) NO(I),SFTAB(IA),BMTAB(IA),THETA(IB-1),DEF(I),
      1 CANOT(I)
      WRITE (6,1030) TITL2
      WRITE(6,1032)
547 WRITE(6,1090) (NO(I),DISTL(I),WTS(I),DISTT(I),CONWT(I),IBRG(I),
      1 I=1,K)
      WRITE(6,1038) WBAR,XBAR
      IXM = IXM
      IF(IXM)1222,1222,980
580 GO TO(1222,1222,1222,1222,1222,1222,981,1221),IXM
      981 CALL GRAPH
560 IF(IXM-7)1222,1222,1221
1222 CONTINUE
      WRITE(6,1036)
      STOP
      END
  
```

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```

$IBFTC RED2 DECK
C READIN MGE2
SUBROUTINE READIN
C KEY FOR IXM SENTINEL
C BLANK ,0 SINGLE CASE, LAST CASE - NO PLOT
C IXM - 1 NEW DENSITY
C 2 NEW DENSITY
C 3 NEW DENSITY AND MODULUS
C 4 MULTIPLE WT RUN - SPEC CASE
C 5,6 SAME AS ,0
C 7 PLOT SINGLE CASE
C 8 PLOT THEN MULTIPLE CASES
C 9 MULTIPLE CASES - ANOTHER FOLLOWS - NO PLOT
C VARIABLE NAMES USED IN READIN DO NOT MATCH REST OF PROGRAM
DIMENSION A(401), B(401), C(401), D(401), E(401), I(401), J(401),
1K(401), L(401), IS(401), H( 7), P( 7), DISTT(401), BMTAB(1620),
2THETA(1802), DEF(401), BNFLU(25,25), DIBRG(25), IBTAB(25), SFTAB(1620),
3TITL2(12), NO(400)
COMMON N,NO,A,B,C,D,E,I,J,K,L,IS,H,P,DISTT,BMTAB,THETA,DEF,
IBNFLU,DIBRG,IBTAB,
2 IBRS,SFTAB,I2,IERROR, TITL2,IXM
DIMENSION NS(50)
COMMON SWAT,NS,IYM
10 FORMAT( 13,5F12.4,2I2,3I1)
15 FORMAT(2I2,2F12.2)
20 FORMAT(17,4F14.4,F14.2,2I6,18,19,I6)
90 FORMAT(25H0 STATION DISTANCE ERROR I5)
91 FORMAT(24I3)
P(6)=-0.0636
P(7)=-0.03705
DO 40 N=1,400
22 READ(5,10)NO(N),A(N),B(N),C(N),D(N),E(N),I(N),J(N),K(N),L(N),IS(N)
IF(NO(N)-900)40,40,45
40 CONTINUE
45 NO(N) = NO(N) -900
51 WRITE(6,20)(NO(I1),A(I1),B(I1),C(I1),D(I1),E(I1),I(I1),

```

RED20002  
 RED20003  
 RED20004  
 RED20005  
 RED20006  
 RED20007  
 RED20008  
 RED20009  
 RED20010  
 RED20011  
 RED20012  
 RED20013  
 RED20014  
 RED20016  
 RED20017  
 RED20018  
 RED20019  
 RED20020  
 RED20021  
 RED20022  
 RED20023  
 RED20024  
 RED20025  
 RED20026  
 RED20027  
 RED20028  
 RED20029  
 RED20030  
 RED20031  
 RED20032  
 RED20033  
 RED20034  
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 RED20036  
 RED20037

RED20038  
RED20039  
RED20040  
RED20041  
RED20042  
RED20043  
RED20044  
RED20045  
RED20046  
RED20047  
RED20048  
RED20049  
RED20050  
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RED20053  
RED20054  
RED20055  
RED20056  
RED20057  
RED20058  
RED20059  
RED20060  
RED20061  
RED20062  
RED20063  
RED20064  
RED20065  
RED20066  
RED20067  
RED20068  
RED20069  
RED20070  
RED20071  
RED20072  
RED20073

```

55      IJ(I1),K(I1),L(I1),IS(I1),I1=1,N)
      PI=3.14159265
      N = N-1
24      READ (5,15) IXM,IYM,AVIT,DAVIT
      IF (IXM) 36,36,27
27      GO TO (29,25,28,81,36,36,36,36,36),IXM
28      H(IYM)=DAVIT
29      P(IYM)=AVIT
      GO TO 24
25      H(IYM)=AVIT
      GO TO 24
81      SWAT=AVIT
C      READ (5,91) (NS(I3),I3=1,IYM)      OPTION NOT ALLOWED IN CURRENT
36      DO 79 I3=1,N
      DISTT(I3)=(A(I3+1))-A(I3))*0.25
      IF (DISTT(I3))82,56,56
      82 WRITE(6,90)NO(I3)
      IERROR = 2
      GO TO 80
56      AREA1=PI*(B(I3)**2-C(I3)**2)/4.0
63      AMI1=PI*(B(I3)**4-C(I3)**4)/64.0
      IMAT=I(I3)
      WT1=AREA1*P(IMAT)
      STIF1=H(IMAT)*AMI1
      ST=STIF1
      WAIT=WT1
      IF (J(I3))65,66,65
65      AREA2=PI*(C(I3)**2-D(I3)**2)/4.0
      AMI2=PI*(C(I3)**4-D(I3)**4)/64.0
      JMAT=J(I3)
      WT2=AREA2*P(JMAT)
      STIF2=H(JMAT)*AMI2
      ST=STIF1+STIF2
      WAIT=WT1+WT2
      IF (L(I3))70,75,70
66      AREA3=PI*(B(I3)**2)/4.0
70

```



RED20074  
RED20075  
RED20076  
RED20077  
RED20078  
RED20079  
RED20080  
RED20081  
RED20082  
RED20083  
RED20084  
RED20085  
RED20086

WT3=AREA3\*P(7)  
WAIT=WAIT-WT3  
IF(I3(I3))77,78,77  
IF(D(I3))68,69,68  
WT4=(PI\*C(I3)\*\*2/4.0)\*P(6)  
GO TO 85  
WT4=(PI\*D(I3)\*\*2/4.0)\*P(6)  
WAIT=WAIT+WT4  
D(I3)=WAIT  
C(I3)=ST  
CONTINUE  
RETURN  
END

75  
77  
69  
68  
85  
78  
79  
80



```

SIBFTC DEFL DECK
SUBROUTINE DEFLN
C DEFLECTION FOR MGE2, MGE5
DIMENSION DISTL(401),DIA(401),STIFX(401),WTS(401),CONWT(401),
1IM(401),JM(401),IBRG(401),IWATR(401),IS(401),YMAT(7),DENMAT(7),
2DISTT(401),BMTAB(1620),THETA(1802),DEF(401),BNFLU(25,25),DIBRG(25)
3,IBTAB(25),SFTAB(1620),TITL2(12),NO(400)
COMMON N,NO,DISTL,DIA,STIFX,WTS,CONWT,IM,JM,IBRG,
1IWATR,IS,YMAT,DENMAT,DISTT,BMTAB,THETA,DEF,BNFLU,DIBRG,IBTAB,
2IBRS,SFTAB,I2,IERROR, TITL2,IXM
DIMENSION NS(50)
COMMON SWAT,NS,IYM
DO 2 I1=1,6
SFTAB(I1)=0.0
BMTAB(I1)=0.0
SFTAB(4)=CONWT(1)
5 DO 40 L=1,N
I=4*L
10 DO 20 J=1,4
MA=I+J
SFTAB(MA)=SFTAB(MA-1)+(WTS(L)*DISTT(L))
20 BMTAB(MA)=(SFTAB(MA-1)+SFTAB(MA))/2.*DISTT(L)+BMTAB(MA-1)
14 SFTAB(MA)=SFTAB(MA)+CONWT(L+1)
40 CONTINUE
DO 30 M=1,N
IK = M+M
I = IK+IK
THETA(IK) =DISTT(M)/3.0*(BMTAB(I)+BMTAB(I+2)+(4.0*BMTAB(I+1)))/
1STIFX(M) +THETA(IK-1)
THETA(IK+1) = DISTT(M)/3.0*(BMTAB(I+2) +BMTAB(I+4)+(4.0*BMTAB(I+3)
1))/STIFX(M)+THETA(IK)
30 DEF(M+1) =2.0/3.0*DISTT(M)*(THETA(IK+1)+THETA(IK-1)+(4.0*THETA(IK)
1)) +DEF(M)
RETURN
END

```

```

$IBFTC BEAM2  DECK
C  SUBROUTINE BEAM
   BEAM SUBROUTINE FOR MGE2 AND MGE5
   COMMON N,NO,DISTL,DIA,STIFX,WTS,CONWT,IM,JM,IBRG,
1  IWATR,IS,YMAT,DENMAT,DISTT,BMTAB,THETA,DEF,BNFLU,DIBRG,IBTAB,
2  IBRS,SFTAB,I2,IERROR,  TITL2,IXM
   DIMENSION DISTL(401),DIA(401),STIFX(401),WTS(401),CONWT(401),
1IM(401),JM(401),IBRG(401),IWATR(401),IS(401),YMAT(7),DENMAT(7),
2DISTT(401),BMTAB(1620),THETA(802),DEF(401),BNFLU(25,25),DIBRG(25)
3,IBTAB(25),SFTAB(1620),TITL2(12),NO(400)
   DIMENSION NS(50)
   COMMON SWAT,NS,IYM
   I1=IBTAB(1)
   ISEND = IBTAB(IBRS)
   CONWT(I1)=(BMTAB(I2)-(SFTAB(I2)*(DISTL(N+1)-DIBRG(IBRS))))/
1(DIBRG(1))-DIBRG(IBRS))
   CONWT(ISEND)=(BMTAB(I2)-(SFTAB(I2)*(DISTL(N+1)-DIBRG(1))))/
1(DIBRG(IBRS))-DIBRG(1))
   RETURN
   END

```

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BEAM0002
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BEAM0019
BEAM0020
BEAM0021

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```

$IBFTC INFN    DECK
C      INFLUENCE NUMBERS FOR MGE2, MGE5
      SUBROUTINE INFNOS
        DIMENSION DISTL(401),DIA(401),STIFX(401),WTS(401),CONWT(401),
        1IM(401),JM(401),IBRG(401),IWATR(401),IS(401),YMAT(7),DENMAT(7),
        2DISTT(401),RMTAB(1620),THETA(802),DEF(401),BNFLU(25,25),DIBRG(25),
        3,IBTAB(25),SFTAB(1620),TITL2(12),NO(400)
        COMMON N,NO,DISTL,DIA,STIFX,WTS,CONWT,IM,JM,IBRG,
        1 IWATR,IS,YMAT,DENMAT,DISTT,BMTAB,THETA,DEF,BNFLU,DIBRG,IBTAB,
        2 IBRS,SFTAB,I2,IERROR,      TITL2,IXM
        DIMENSION NS(50)
        COMMON SWAT,NS,IYM
        N1=3
        NTWO = N+N
        NFOR = NTWO+NTWO
        DO 99 I1=1,N
          N2=2
          IF (IBRG(I1)) 60,99,60
60      DO 63 I3=1,N
63      DEF(I3)=0.0
        DO 64 I32=1,NTWO
64      THETA(I32)=0.0
        DO 65 I34=1,NFOR
65      BMTAB(I34)=0.0
        DO 95 J1=I1,N
          I4=4*J1
          DO 75 J2=1,I4
            K1=I4+J2
75      BMTAB(K1)=DISTT(J1)+BMTAB(K1-1)
            K2=2*J1
            THETA(K2)=DISTT(J1)*(BMTAB(K1-4)+BMTAB(K1-2)+(4.0*BMTAB(K1-3)))/(SINFN0031
            1TIFX(J1)*3.0) +THETA(K2-1)
            THETA(K2+1)=DISTT(J1)*(BMTAB(K1)+BMTAB(K1-2)+(4.0*BMTAB(K1-1)))/(SINFN0033
            1TIFX(J1)*3.0) +THETA(K2)
95      DEF(J1)=(2.0/3.0)*DISTT(J1)*(THETA(K2+1)+THETA(K2-1)+(4.0*THETA(K2)
            1)) ) +DEF(J1-1)

```



```

DO 97 J3=1,N
IF (IBRG(J3)) 96,97,96
96 BNFLU(N1,N2)=DEF(J3-1)
N2=N2+1
97 CONTINUE
N1=N1+1
99 CONTINUE
100 RETURN
END

```

A. 12

```

INFN0037
INFN0038
INFN0039
INFN0040
INFN0041
INFN0042
INFN0043
INFN0044
INFN0045

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```

$IBFTC INOU DECK
C SUBROUTINE INOUT
  INOUT FOR MGE2, MGE5
  DIMENSION DISTL(401),DIA(401),STIFX(401),WTS(401),CONWT(401),
  IIM(401),JM(401),IBRG(401),IWATR(401),IS(401),YMAT(7),DENMAT(7),
  2DISTT(401),BMTAB(1620),THETA(802),DEF(401),BNFLU(25,25),DIBRG(25)
  3,IBTAB(25),SFTAB(1620),TITL2(12),NO(400)
  COMMON N,NO,CISTL,DIA,STIFX,WTS,CONWT,IM,JM,IBRG,
  1 IWATR,IS,YMAT,DENMAT,DISTT,BMTAB,THETA,DEF,BNFLU,DIBRG,IBTAB,
  2 IBRS,SFTAB,I2,IERROR, TITL2,IXM
  DIMENSION NS(50)
  COMMON SWAT,N,S,IYM
  IBRS = 0
  DO 2 I1=1,22
    2 IBTAB(I1) = 0.0
    DO 70 I1=1,N
      IF (IBRG(I1)) 70,70,65
      65 IBRS = IBRS +1
      IBTAB(IBRS) = I1
      DIBRG(IBRS) = DISTL(I1)
    70 CONTINUE
    IBR1=IBRS+1
    IBR2=IBRS+2
    BNFLU(1,1) = 0.0
    BNFLU(2,1) = 0.0
    BNFLU(1,IBR2) = 0.0
    BNFLU(2,IBR2) = 0.0
    DO 102 J5=2,IBR1
      BNFLU(1,J5)=1.0
      BNFLU(2,J5)=DIBRG(J5-1)
      BNFLU(J5+1,1) = DIBRG(J5-1)
      BNFLU(J5+1,IBR2) = 1.0
    102 CONTINUE
    CALL MATINV(BNFLU,IBR2,STOR,0,DETERM,ID)
    GO TO (221,610), ID
    231 DO 600 K7= 1,IBRS

```

A. 13

BEST AVAILABLE COPY

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1 INOU0002
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INOU0035
INOU0036

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INOU0037  
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 INOU0047  
 INOU0048  
 INOU0049  
 INOU0050

```

    NK7 = IBRS-K7+1
    BNFLU(25,NK7) = BNFLU(NK7+1,2)
    BNFLU(24,NK7) = BNFLU(NK7+1,1)
    DO 236 K8 = 1,IBRS
    DO 236 K7 = 1,IBRS
    BNFLU(K7,K8) = BNFLU(K7+1,K8+2) *.001
    236 CONTINUE
    550 CONTINUE
    551 RETURN
    C  ERROR SET FOR SINGULAR ARRAY
    610 WRITE(6,611)
    611 FORMAT(29H0 SINGULAR INFLUENCE NUMBERS ///)
    IERROR = 2
    GO TO 551
    END
  
```



```

SIBFTC MAT2    DECK
C    MATRIX INVERSION WITH ACCOMPANYING SOLUTION OF LINEAR EQUATIONS
C    INTERNAL DOUBLE PRECISION      PIVOT METHOD
C    NOVEMBER 1692    S GOOD  DAVID TAYLOR MODEL BASIN    AM MAT2
C
C    SUBROUTINE MATINV(A,N1,B,M1,DETERM,ID)
C
C    GENERAL FORM OF DIMENSION STATEMENT
C    DIMENSION  A( , ),B( , ),INDEX( ,3),A1( , ),B1( , )
C
C    DIMENSION  A(25,25),B( 1, 1),INDEX(25,3) ,A1(25,25),B1(1,1)
C    EQUIVALENCE (IROW,JROW), (ICOLUMN,JCOLUMN), (AMAX, T, SWAP)
C    EQUIVALENCE (T4,PIVOT1),(T5,PIVOT)
C
C    INITIALIZATION
C
C    N=N1
C    M=M1
C    10 DETERM=1.0
C       D TERM1=0.0
C    15 DO 20 J=1,N
C       DO 17 I=1,N
C    17 A1(J,I) = 0.0
C       IF(M) 20,20,19
C    19 DO 18 I =1,M
C    18 B1(J,I) = 0.0
C    20 INDEX(J,3) = 0
C    30 DO 550 I=1,N
C
C    SEARCH FOR PIVOT ELEMENT
C
C    40 AMAX=0.0
C    45 DO 105 J=1,N
C       IF(INDEX(J,3)-1) 60, 105, 60
C    60 DO 100 K=1,N
C       IF(INDEX(K,3)-1) 80, 100, 715

```

# BEST AVAILABLE COPY

MAT20037  
MAT20038  
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MAT20070  
MAT20071

```

80 IF (AMAX-ABS(A(J,K)))85,100,100
85 IROW=J
90 ICOLUM=K
   AMAX=ABS(A(J,K))
100 CONTINUE
105 CONTINUE
   INDEX(ICOLUM,3) = INDEX(ICOLUM,3) +1
260 INDEX(I,1)=IPOW
270 INDEX(I,2)=ICOLUM
C
C   INTERCHANGE ROWS TO PUT PIVOT ELEMENT ON DIAGONAL
C
130 IF (IROW-ICOLUM) 140, 310, 140
140 DETERM=-DETERM
   D TERM1=-D TERM1
150 DO 200 L=1,N
   SWAP=A1(IROW,L)
   A1(IROW,L)=A1(ICOLUM,L)
   A1(ICOLUM,L)=SWAP
160 SWAP=A(IROW,L)
170 A(IROW,L)=A(ICOLUM,L)
200 A(ICOLUM,L)=SWAP
   IF(M) 310, 310, 210
210 DO 250 L=1, M
   SWAP =B1(IROW,L)
   B1(IROW,L)=B1(ICOLUM,L)
   B1(ICOLUM,L)=SWAP
220 SWAP=B(IROW,L)
230 B(IROW,L)=B(ICOLUM,L)
250 B(ICOLUM,L)=SWAP
C
C   DIVIDE PIVOT ROW BY PIVOT ELEMENT
C
310 PIVOT =A(ICOLUM,ICOLUM)
   PIVOT1 =A1(ICOLUM,ICOLUM)
320 CALL FMP(DETERM,D TERM1,PIVOT ,PIVOT1 ,DETERM,D TERM1)

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MAT20072  
MAT20073  
MAT20074  
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MAT20099  
MAT20100  
MAT20101  
MAT20102  
MAT20103  
MAT20104  
MAT20105  
MAT20106  
MAT20107

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330 A(ICOLUMN,ICOLUMN)=1.0
    A1(ICOLUMN,ICOLUMN)=0.0
340 DO 350 L=1,N
350 CALL FDY(A(ICOLUMN,L),A1(ICOLUMN,L),PIVOT ,PIVOT1 ,
    A(ICOLUMN,L),A1(ICOLUMN,L))
355 IF(M) 380, 380, 360
360 DO 370 L=1,M
370 CALL FDY(B(ICOLUMN,L),B1(ICOLUMN,L),PIVOT ,PIVOT1 ,
    B(ICOLUMN,L),B1(ICOLUMN,L))
    C
    C
    C
    REDUCE NON-PIVOT ROWS
380 DO 550 L1=1,N
390 IF(L1-ICOLUMN) 400, 550, 400
400 T=A(L1,ICOLUMN)
    T1 = A(L1,ICOLUMN)
420 A(L1,ICOLUMN)=0.0
    A1(L1,ICOLUMN) = 0.0
430 DO 450 L=1,N
    CALL FMP (T,T1,A(ICOLUMN,L),A1(ICOLUMN,L),T4,T5)
450 CALL FSB (A(L1,L),A1(L1,L),T4,T5,A(L1,L),A1(L1,L))
455 IF(M) 550, 550, 460
460 DO 500 L=1,M
    CALL FMP (T,T1,B(ICOLUMN,L),B1(ICOLUMN,L),T4,T5)
500 CALL FSB (B(L1,L),B1(L1,L),T4,T5,B(L1,L),B1(L1,L))
550 CONTINUE
    C
    C
    C
    INTERCHANGE COLUMNS
600 DO 710 I=1,N
610 L=N+1-I
620 IF (INDEX(L,1)-INDEX(L,2)) 630, 710, 630
630 JROW=INDEX(L,1)
640 JCOLUMN=INDEX(L,2)
650 DO 705 K=1,N
    SWAP = A1(K,JROW)

```



MAT20108  
 MAT20109  
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 MAT20122  
 MAT20123  
 MAT20124

```

    A1(K,JROW) = A1(K,JCOLUMN)
    A1(K,JCOLUMN) = SWAP
    660 SWAP=A(K,JROW)
    670 A(K,JROW)=A(K,JCOLUMN)
    700 A(K,JCOLUMN)=SWAP
    705 CONTINUE
    710 CONTINUE
    DO 730 K = 1,N
    IF(INDEX(K,3) -1) 715,720,715
    715 ID =2
    GO TO 740
    720 CONTINUE
    730 CONTINUE
    ID =1
    740 RETURN
    C    LAST CARD OF PROGRAM
    END
  
```

\$IBMAP	DPAF	DECK	FORTRAN	PACKAGE	7090	BE	SYS3
*	DOUBLE PRECISION						
	ENTRY	FAD					
	ENTRY	FSB					
	ENTRY	FMP					
	ENTRY	FDY					
	ENTRY	TEST					
FAD	SXA	END+2,2					
	TXI	*+1,4,-2					
	TSX	ALL,2					
	CLA	COMMON+2	B1				
FADE	FAD	COMMON	A1				
	STO	COMMON					
	CLA	COMMON+1	A2				
	STQ	COMMON+1					
	FAD	COMMON+3					
	FAD	COMMON+1	B2				
	FAD	COMMON					
END	STO*	5,4					
	STQ*	6,4					
	AXT	**2					
	TRA	7,4					
FSB	SXA	END+2,2					
	TXI	*+1,4,-2					
	TSX	ALL,2					
	CLS	COMMON+3					
	STO	COMMON+3					
	CLS	COMMON+2					
	TXL	FADE, **					
ALL	CLA*	1,4					
	STO	COMMON					
	CLA*	2,4					
	STO	COMMON+1					
	CLA*	3,4					
	STO	COMMON+2					
	CLA*	4,4					

CHANGE SIGN B AND ADD

SECURE INPUTS AND OUTPUT

DPAF0001  
 DPAF0002  
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DPAF0059  
DPAF0060  
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DPAF0062  
DPAF0063  
DPAF0064  
DPAF0065  
DPAF0066  
DPAF0067  
DPAF0068  
DPAF0069  
DPAF0070  
DPAF0071  
DPAF0072

STO COMMON+3  
TRA 1,2  
SXA END+2,2  
TXI \*+1,4,-2  
TSX ALL,2  
LDQ COMMON  
FMP COMMON+3  
STO COMMON+3  
LDQ COMMON  
FMP COMMON+2  
STQ COMMON  
LDQ COMMON+1  
STO COMMON+1  
FMP COMMON+2  
FAD COMMON+3  
FAD COMMON  
FAD COMMON+1  
TRA END  
SXA END+2,2  
TXI \*+1,4,-2  
TSX ALL,2  
CLA COMMON  
FDP COMMON+2  
STQ COMMON  
FAD COMMON+1  
FDP COMMON+2  
STQ COMMON+1  
CLA COMMON+3  
ANA FDYC  
FSB COMMON+3  
FDP COMMON+2  
FMP COMMON  
FAD COMMON+1  
FAD COMMON  
DCT  
TRA ERR

FMP

FDY

A. 20

A1 TIMES B2  
A1 TIMES B1  
A2 TIMES B1  
A1 OVER B1  
REMAINDER A1 OVER B1 + A2  
DIVIDE BY B1  
ISOLATE POWER  
-B2 OVER B1  
TIMES A1 OVER B1  
ADD LESSER PARTS  
ADD A1 OVER B1



DPAF0073  
DPAF0074  
DPAF0075  
DPAF0076  
DPAF0077  
DPAF0078  
DPAF0079  
DPAF0080  
DPAF0081  
DPAF0082  
DPAF0083  
DPAF0084  
DPAF0085  
DPAF0086  
DPAF0087  
DPAF0088  
DPAF0089  
DPAF0090  
DPAF0091  
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DPAF0094  
DPAF0095  
DPAF0096  
DPAF0097  
DPAF0098  
DPAF0099  
DPAF0100  
DPAF0101  
DPAF0102  
DPAF0103  
DPAF0104

TRA END  
FDYC OCT 377000000000  
TEST LDQ TESTC  
TXI \*+1,4,-2  
STQ END  
TRA FSB  
TESTR LDQ TESTC+1  
STQ END  
TMI TESTX+2  
FSB\* 5,4  
TMI TESTX+4  
CLA ERR-1  
TESTX LXA END+2,2  
TRA 6,4  
FAD\* 5,4  
TMI TESTX+6  
ZAC  
TRA TESTX  
CLS ERR-1  
TRA TESTX  
DEC 1.  
ERR SXA ERR+4,4  
TSX \*MWR,4  
PZE 1 7/14/64  
PZE FORM,5  
AXT \*\*,4  
TRA END  
FORM BCI 5, DBL PREC DIV CKECK  
TESTC TRA TESTR  
STO\* 5,4  
COMMON BSS 4  
END

PLUS ONE

ZEERO

MINUS ONE

MAP

PRINT BUT PROCEED

```

$IBFTC GRAPH2 DECK
SUBROUTINE GRAPH
C DIMENSION AS IN MGE2
  DIMENSION DISTL(401),DIA(401),STIFX(401),WTS(401),CONWT(401),
  1IM(401),JM(401),IBRG(401),IWATR(401),IS(401),YMAT(7),DENMAT(7),
  2DISTT(401), BMTAB(1620),THETA(802),DEF(401),BNFLU(25,25),DIBRG(25)
  3,IBTAB(25), SFTAB(1620),TITL2(12),NO(400)
C COMMON AS IN MGE2
  COMMON N,NO,DISTL,DIA,STIFX,WTS,CONWT,IM,JM,IBRG,
  2 IBRS,SFTAB,I2,IERROR, TITL2,IXM
  DIMENSION IPLT(23), GTITLE (21)
  DATA GTITLE(1)/6H(74H /
  CALL LGCHAR (8,4HMG2)
  K=N+1
  DO 30 I=1,K
    30 BMTAB(I)= BMTAB(4*I)/1000.
    PLOT1=450.
    I5=1
    IGP=9
    IGS.= 1
    IFF=1
    DO1 IF=1,23
      IPLT(IF)=0
    1 COLLECT BEARING POINTS FOR PLOT
    DO2 I3=1, IBRS
      I4 = IBTAB(I3)
      BNFLU (I3,1)= DISTL(I4)
      BNFLU (I3,2)= DEF (I4)
      22 BNFLU (I3,3)=BMTAB (I4)
      IF(K-99 ) 5, 5 , 4
      5 PLOT1 =AINT ((DISTL(K)+99.)/100.)*100.
      IPLT(2)=K
      IFF=1
      IGP = (PLOT1+99.)*.01
      IGS = 2
      IF(IGP-35) 9,9,19

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GRAP0001
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GRAP0037

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GRAP0038  
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GRAP0067  
GRAP0068  
GRAP0069  
GRAP0070  
GRAP0071  
GRAP0072  
GRAP0073

```

19 IGP = (IGP+1)/2
   GO TO 9
4   DO 2 IF=1,K
   IF(DISTL(IF)-PLOT1) 2, 2, 3
3   IPLT(IFF+1)= IF-1
   IFF= IFF+1
   PLOT1=PLOT1+450.
2   CONTINUE
   IPLT(IFF+1)=K
   HAVE NO OF FRAMES SET UP
   PLOT1 = 450.0
   COMPUTE SCALES FOR DEFL. AND BEND. MOMENT
9   GDEF=0.
   DO 6 I=1,K
8   IF(ABS (DEF(I))-GDEF) 6, 6, 8
   GDEF = ABS (DEF(I))
6   CONTINUE
   GBML = 0.
   GBMH = 0.
   DO 12 I=1,K
10  IF (BMTAB(I)) 10,12, 11
13  IF (BMTAB(I)-GBML) 13,12,12
   GBML=BMTAB(I)
   GO TO 12
11  IF (BMTAB(I) -GBMH) 12, 12,14
14  GBMH = BMTAB(I)
12  CONTINUE
   GBML=100. *AINT ((GBML -99.)/100.)
   GBMH=100. *AINT ((GBMH +99.)/100.)
   IGBMD=(GBMH-GBML +99.)*.01
   IF(IGBMD-35)24,24,25
25  IGBMD = (IGBMD+1)/2
24  IF(IGBMD-10) 15,15, 16
15  IGBMD = IGBMD +IGBMD
16  GDEF=AINT ((GDEF +.0099)*100.) *.01
   IGDEF = (GDEF+GDEF+.009)*100.

```



GRAP0074  
GRAP0075  
GRAP0076  
GRAP0077  
GRAP0078  
GRAP0079  
GRAP0080  
GRAP0081  
GRAP0082  
GRAP0083  
GRAP0084  
GRAP0085  
GRAP0086  
GRAP0087  
GRAP0088  
GRAP0089  
GRAP0090  
GRAP0091  
GRAP0092  
GRAP0093  
GRAP0094  
GRAP0095  
GRAP0096  
GRAP0097  
GRAP0098  
GRAP0099  
GRAP0100  
GRAP0101  
GRAP0102  
GRAP0103  
GRAP0104  
GRAP0105  
GRAP0106  
GRAP0107  
GRAP0108  
GRAP0109

```

17 IF(IGDEF -10) 17,17,18
18 IGDEF = ICDEF + IGDEF
19 IF(IGDEF-35) 26,26,23
23 IGDEF = (:GDEF+1)/2
26 CONTINUE
DO 7 IG=1,20
GTITLE(IG+1) = TTTL2(IG)
PLOTB=PLOT1
PLOTB=0.
DO 20 IC=1,IFF
IST = IPLT(IC)
ISH = IPLT(IC+1)-IST
CALL FNPLOT( GTITLE( 1),32H(28H SECTION DISTANCE IN INCHES,
132H(28H BENDING MOMENT IN KIP FEET,PLOTA,PLOTB, GBML,GBMH,IGP,
2 IGS, IGBMD,2 , 6H(F7.1), 6H(F7.0))
CALL CURVE (DISTL(IST), BMTAB(IST) , ISH, 6H
I4=0
DO41 I3=I5,IBRS
IF(1BTAB(I3)-IST) 40,40,50
I4=I4+1
CONTINUE
I5=IBRS+1
GO TO 51
I5=I3
50 IF(I4) 52,52,53
51 GET BEARING VALUES ON DEFL PLOT
CALL CURVE (BNFLU( 1,1),BNFLU( 1,3),I4 ,6H 0)
PLOTA=PLOTB
PLOTB=PLOTB+450.
PLOTB=PLOT1
I5 = 1
PLOTA=0.
DO 21 IC =1,IFF
IST = IPLT(IC)
ISH = IPLT(IC+1)-IST
CALL FNPLOT( GTITLE( 1),32H(28H SECTION DISTANCE IN INCHES,

```

```

126H(22H DEFLECTION IN INCHES , PLOTA,PLOTB,-GDEF,GDEF,IGP,IGS,
2  IGDEF,2, 6H(F7.1),6H(F6.3))
  CALL CURVE (DISTL(IST), DEF (IST) , ISH , 6H )
  I4=0
DO 43 I3=I5,IBRS
IF (IBTAB(I3)-IST)44,44,45
44 I4=I4+1
43 CONTINUE
  I5=IBRS+1
  GO TO 46
45 I5=I3
46 IF (I4) 54,54 ,55
55 CALL CURVE (BNFLU( 1,1), BNFLU( 1,2), I4 ,6H 0)
54 PLOTA=PLOTB
21 PLOTB=PLOTB+450.
  CALL LGCHAR (8, 4H2END)
  RETURN
  END
GRAP0110
GRAP0111
GRAP0112
GRAP0113
GRAP0114
GRAP0115
GRAP0116
GRAP0117
GRAP0118
GRAP0119
GRAP0120
GRAP0121
GRAP0122
GRAP0123
GRAP0124
GRAP0125
GRAP0126
GRAP0127

```







MAT2L037  
MAT2L038  
MAT2L039  
MAT2L040  
MAT2L041  
MAT2L042  
MAT2L043  
MAT2L044  
MAT2L045  
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MAT2L066  
MAT2L067  
MAT2L068  
MAT2L069  
MAT2L070  
MAT2L071  
MAT2L072

```

85 IROW=J
90 ICOLUM=K
   AMAX = ABSF(A(J,K))
100 CONTINUE
105 CONTINUE
   INDEX(ICOLUM,3) = INDEX(ICOLUM,3) +1
260 INDEX(I,1)=IROW
270 INDEX(I,2)=ICOLUM
C
C   INTERCHANGE ROWS TO PUT PIVOT ELEMENT ON DIAGONAL
C
130 IF (IROW-ICOLUM) 140, 310, 140
140 DETERM=-DETERM
150 DO 200 L=1,N
160 SWAP=A(IROW,L)
170 A(IROW,L)=A(ICOLUM,L)
200 A(ICOLUM,L)=SWAP
   IF(M) 310, 310, 210
210 DO 250 L=1, M
220 SWAP=B(IROW,L)
230 B(IROW,L)=B(ICOLUM,L)
250 B(ICOLUM,L)=SWAP
C
C   DIVIDE PIVOT ROW BY PIVOT ELEMENT
C
310 PIVOT =A(ICOLUM,ICOLUM)
   DETERM=DETERM*PIVOT
330 A(ICOLUM,ICOLUM)=1.0
340 DO 350 L=1,N
350 A(ICOLUM,L)=A(ICOLUM,L)/PIVOT
355 IF(M) 380, 380, 360
360 DO 370 L=1,M
370 B(ICOLUM,L)=B(ICOLUM,L)/PIVOT
C
C   REDUCE NON-PIVOT ROWS
C

```

MAT2L073  
 MAT2L074  
 MAT2L075  
 MAT2L076  
 MAT2L077  
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 MAT2L103  
 MAT2L104  
 MAT2L105  
 MAT2L106  
 MAT2L107  
 MAT2L108

```

380 DO 550 L1=1,N
390 IF(L1-ICOLUM) 400, 550, 400
400 T=A(L1,ICOLUM)
420 A(L1,ICOLUM)=0.0
430 DO 450 L=1,N
450 A(L1,L)=A(L1,L)-A(ICOLUM,L)*T
455 IF(M) 550, 550, 460
460 DO 500 L=1,M
500 B(L1,L)=B(L1,L)-B(ICOLUM,L)*T
550 CONTINUE

C
C INTERCHANGE COLUMNS
C
600 DO 710 I=1,N
610 L=N+1-I
620 IF (INDEX(L,1)-INDEX(L,2)) 630, 710, 630
630 JROW=INDEX(L,1)
640 JCOLUM=INDEX(L,2)
650 DO 705 K=1,N
660 SWAP=A(K,JROW)
670 A(K,JROW)=A(K,JCOLUM)
700 A(K,JCOLUM)=SWAP
705 CONTINUE
710 CONTINUE
DO 730 K = 1,N
IF(INDEX(K,3) -1) 715,720,715
715 ID =2
GO TO 810
720 CONTINUE
730 CONTINUE
ID =1
740 DO 800 J=1,N
DO 801 I =1,N
801 A(I,J) = A(I,J)
IF(M) 800,800,802
802 DO 803 I =1,M

```



MAT2L109  
MAT2L110  
MAT2L111  
MAT2L112  
MAT2L113

803 B1(J,I) = 5(J,I)  
800 CONTINUE  
DTERM1 = DETERM  
810 RETURN  
C LAST CARD OF PROGRAM  
END



# MGE2 - SAMPLE INPUT FORM

COLUMN	1	2	4	5	7
1 3 5	6	8	C	2	3
SAMPLE CASE	12 BEARING SHAFT	4/1/64			
01 0.0	8.0				TMGE
02 2.0	8.0				TMGE
03 4.0	18.0				TMGE
04 12.5	18.0				TMGE
05 24.0	36.0				TMGE
06 40.5	36.0				TMGE
07 57.25	18.0				TMGE
08 68.5	18.0				TMGE
09 93.5	33.0				TMGE
10 98.5	18.0				TMGE
11 109.5	17.5				TMGE
12 122.75	31.0				TMGE
13 130.25	17.0				TMGE
14 306.5	17.0				TMGE
15 540.5	17.0				TMGE
16 590.75	31.0				TMGE
17 598.25	17.0				TMGE
18 774.5	17.0				TMGE
19 1008.5	17.0				TMGE
20 1058.75	31.0				TMGE
21 1066.25	17.0				TMGE
22 1242.5	17.0				TMGE
23 1476.5	17.0				TMGE
24 1526.75	31.0				TMGE
25 1534.25	17.0				TMGE
26 1698.50	17.0				TMGE
27 1914.5	17.0				TMGE

28 1968.5	34.0		3		TMGE
29 2028.5	19.5625		3	1	TMGE
30 2082.5	21.8125	19.5625	2	3 1	TMGE
31 2121.5	21.8125	19.5625	2	111	TMGE
32 2160.5	21.375	19.5625	2	101	TMGE
33 2371.0	21.8125	19.5625	2	101	TMGE
34 2443.0	21.8125	19.5625	2	311	TMGE
35 2515.0	19.5625		3	1	TMGE
36 2543.5	19.5625		3	1	TMGE
37 2559.5	16.0		3	1	TMGE
938 2571.5					TMGE
3 3 -0.28355	30000000.				TMGE
07					TMGE

-24343.0

Note: Material 3 as used is identical to Material 1 to illustrate the insertion of new material cards.



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## MGE2 - SAMPLE OUTPUT SHEETS

\*\*\* SHAFTING SYSTEM PROGRAM MGE2 \*\*\*

SAMPLE CASE 12 BEARING SHAFT 1/1/63 1

STATION NO.	SECTION DISTANCE (INCH)	INPUT DATA				MATERIALS		BEARING POSITION	IN WATER	WITH SAND
		FIRST DIAMETER (INCH)	SECOND DIAMETER (INCH)	THIRD DIAMETER (INCH)	CONCENTRATED WEIGHT (LB.)	A	B			
1	0.	8.0000	-0.	-0.	-0.	3	-0	-0	-0	-0
2	2.0000	8.0000	-0.	-0.	-0.	3	-0	-0	-0	-0
3	4.0000	18.0000	-0.	-0.	-0.	3	-0	-0	-0	-0
4	12.5000	18.0000	-0.	-0.	-0.	1	-0	1	-0	-0
5	24.0000	36.0000	-0.	-0.	-0.	1	-0	-0	-0	-0
6	46.5000	36.0000	-0.	-0.	-23100.00	1	-0	-0	-0	-0
7	57.2500	18.0000	-0.	-0.	-0.	1	-0	-0	-0	-0
8	68.5000	18.0000	-0.	-0.	-0.	3	-0	1	-0	-0
9	93.5000	33.0000	-0.	-0.	-0.	3	-0	-0	-0	-0
10	98.5000	18.0000	-0.	-0.	-0.	3	-0	-0	-0	-0
11	109.5000	17.5000	-0.	-0.	-0.	3	-0	-0	-0	-0
12	122.7500	31.0000	-0.	-0.	-0.	3	-0	-0	-0	-0
13	130.2500	17.0000	-0.	-0.	-0.	3	-0	-0	-0	-0
14	306.5000	17.0000	-0.	-0.	-0.	1	-0	1	-0	-0
15	540.5000	17.0000	-0.	-0.	-0.	3	-0	1	-0	-0
16	590.7500	31.0000	-0.	-0.	-0.	3	-0	-0	-0	-0
17	598.2500	17.0000	-0.	-0.	-0.	3	-0	-0	-0	-0
18	774.5000	17.0000	-0.	-0.	-0.	1	-0	-0	-0	-0
19	1008.5000	17.0000	-0.	-0.	-0.	3	-0	1	-0	-0
20	1058.7500	31.0000	-0.	-0.	-0.	3	-0	-0	-0	-0
21	1066.2500	17.0000	-0.	-0.	-0.	3	-0	-0	-0	-0
22	1242.5000	17.0000	-0.	-0.	-0.	1	-0	1	-0	-0
23	1476.5000	17.0000	-0.	-0.	-0.	3	-0	1	-0	-0
24	1526.7500	31.0000	-0.	-0.	-0.	3	-0	-0	-0	-0
25	1534.2500	17.0000	-0.	-0.	-0.	3	-0	-0	-0	-0
26	1698.5000	17.0000	-0.	-0.	-0.	1	-0	1	-0	-0
27	1914.5000	17.0000	-0.	-0.	-0.	3	-0	1	-0	-0
28	1968.5000	34.0000	-0.	-0.	-0.	3	-0	-0	-0	-0
29	2026.5000	19.5625	-0.	-0.	-0.	3	-0	-0	-0	-0
30	2082.5000	21.8125	19.5625	-0.	-0.	2	3	-0	1	-0
31	2121.5000	21.8125	19.5625	-0.	-0.	2	1	-0	1	-0
32	2160.5000	21.3780	19.5625	-0.	-0.	2	1	0	1	-0
33	2371.0000	21.8125	19.5625	-0.	-0.	2	1	0	1	-0
34	2443.0000	21.8125	19.5625	-0.	-0.	2	3	1	1	-0
35	2515.0000	19.5625	-0.	-0.	-0.	3	-0	-0	1	-0
36	2543.5000	19.5625	-0.	-0.	-24343.00	3	-0	-0	1	-0
37	2559.5000	16.0000	-0.	-0.	-0.	3	-0	-0	1	-0
38	2571.5000	-0.	-0.	-0.	-0.	3	-0	-0	0	-0

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SAMPLE CASE		12 BEARING SHAFT	1/1/63	1
UNDRFLOW AT 13633 IN MQ				
UNDRFLOW AT 13624 IN MQ				
UNDRFLOW AT 13633 IN MQ				
UNDRFLOW AT 13634 IN MQ				
UNDRFLOW AT 13635 IN MQ				
DEFLECTION AND SLOPE	INFLUENCE NUMBERS ON STATION 1	(FOR ONE INCH OF RISE OF BEARING)		
BRG. NO.	DEFLECTION	SLOPE		
1	1.2301325	-0.01841060		
2	-0.2321747	0.01857397		
3	0.0025792	-0.00020633		
4	-0.0006828	0.00005462		
5	0.0001842	-0.00001474		
6	-0.0000489	0.00000390		
7	0.0000132	-0.00000105		
8	-0.0000036	0.00000028		
9	0.0000010	-0.00000008		
10	-0.0000003	0.00000002		
11	0.0000001	-0.00000000		
12	-0.0000000	0.00000000		



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SAMPLE CASE 12 BEARING SHAFT 1/1/63 1  
BEARING REACTION INFLUENCE NUMBERS (LB. PER 0.001 INCM RISE OF BEARING)

BRG. NO.	1	2	3	4	5	6	7	8	9	10	11
1	622.0	-805.6	231.9	-61.4	16.6	-4.4	1.2	-0.3	0.1	-0.0	0.0
2	-805.6	1058.3	-334.5	104.0	-28.1	7.4	-2.0	0.5	-0.2	0.0	-0.0
3	231.9	-334.5	130.7	-114.9	46.5	-12.3	3.3	-0.9	0.3	-0.1	0.0
4	-61.4	104.0	-114.9	142.7	-104.7	43.5	-11.8	3.2	-0.9	0.3	-0.1
5	16.6	-28.1	46.5	-104.7	139.5	-104.4	43.8	-11.9	3.5	-1.0	0.2
6	-4.4	7.4	-12.3	43.5	-104.4	140.1	-104.3	44.4	-12.9	3.7	-0.9
7	1.2	-2.0	3.3	-11.8	43.8	-104.3	140.5	-108.3	48.3	-13.8	3.4
8	-0.3	0.5	-0.9	3.2	-11.9	44.4	-108.3	152.7	-121.8	94.7	-13.6
9	0.1	-0.2	0.3	-0.9	3.5	-12.9	48.3	-121.8	178.7	-141.8	53.6
10	-0.0	0.0	-0.1	0.3	-1.0	3.7	-13.8	84.7	-141.8	210.5	-143.1
11	0.0	-0.0	0.0	-0.1	0.2	-0.9	3.4	-13.6	53.6	-143.1	142.4
12	-0.0	0.0	-0.0	0.0	-0.0	0.1	-0.3	1.2	-4.8	30.6	-42.0

A. 34

STRAIGHT LINE BEARING REACTIONS (LBS.)

11222.6	33679.8	15265.7	15996.5	15230.3	15997.3	15278.8	15845.6	13430.6	23299.6	15898.3
---------	---------	---------	---------	---------	---------	---------	---------	---------	---------	---------

BRG. NO.	12	13	14	15	16	17	18	19	20	21	22
1	-0.0										
2	0.0										
3	-0.0										
4	0.0										
5	-0.0										
6	0.1										
7	-0.3										
8	1.2										
9	-4.8										
10	30.6										
11	-42.0										
12	15.2										

STRAIGHT LINE BEARING REACTIONS (LBS.)

89400.6

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SAMPLE CASE 12 BEARING SHAFT 1/1/63

STATION NO.	SHEAR FORCE (KIP.)	MOMENT (KIP-INCH)	SHAFTING SECTION INTEGRALS	DEFLECTION (INCH)	BEARING REACTION (LBS.)
1	-0.	0.	SLOPE (RADIAN)	0.0000383	0.
2	-0.02851	-0.029	-0.0000030	-0.0000382	0.
3	-0.05701	-0.114	-0.0000031	0.0000262	0.
4	10.55231	-3.205	-0.0000031	-0.0000000	11228.6
5	9.72253	113.375	0.0000010	-0.0000203	0.
6	-18.13968	234.509	0.0000022	0.0000085	0.
7	-22.97404	-109.819	0.0000027	-0.0000601	0.
8	9.89397	-372.843	-0.0000148	-0.0000000	32479.2
9	8.09011	-148.042	-0.0000363	-0.0000647	0.
10	6.87751	-110.623	-0.0000567	-0.0012472	0.
11	6.08381	-39.335	-0.0000620	-0.0019045	0.
12	5.18013	35.288	-0.0000621	-0.0027341	0.
13	3.57502	68.120	-0.0000618	-0.0031986	0.
14	7.49728	-301.426	0.0000098	-0.0000000	18288.7
15	6.43347	-309.116	-0.0000122	-0.0000003	18994.5
16	5.19337	33.409	-0.0000630	-0.0024780	0.
17	3.59426	66.385	-0.0000528	-0.0029498	0.
18	7.49003	-299.772	0.0000088	-0.0006011	18239.3
19	8.42703	-309.158	-0.0000118	-0.0000028	18997.3
20	5.19293	33.043	-0.0000528	-0.0024473	0.
21	3.58783	65.971	-0.0000523	-0.0029261	0.
22	7.52315	-301.319	0.0000078	-0.0000058	18278.2
23	8.30847	-302.955	-0.0000083	-0.0000198	18248.2
24	5.07437	33.288	-0.0000579	-0.0022493	0.
25	3.46926	65.327	-0.0000576	-0.0028829	0.
26	6.33671	-233.004	0.0000237	-0.0000171	18438.6
27	15.73454	-365.669	-0.0000526	-0.0000260	23299.6
28	12.25909	390.159	-0.0000503	-0.0045678	0.
29	-3.18736	662.311	-0.0000319	-0.0070772	0.
30	-7.18818	382.171	0.0001033	-0.0048337	0.
31	5.03098	30.088	0.0001343	-0.0000358	15998.3
32	1.35180	154.552	0.0001491	0.0054330	0.
33	-17.64124	-1559.911	-0.0001483	0.0297298	0.
34	35.02704	-3074.604	-0.0007453	-0.0000569	59400.6
35	28.23470	-797.181	-0.0012424	-0.0752001	0.
36	1.78016	-22.582	-0.0012959	-0.1116143	0.
37	0.59473	-3.583	-0.0012968	-0.1323578	0.
38	-0.00001	-0.015	-0.0012969	-0.1479202	0.



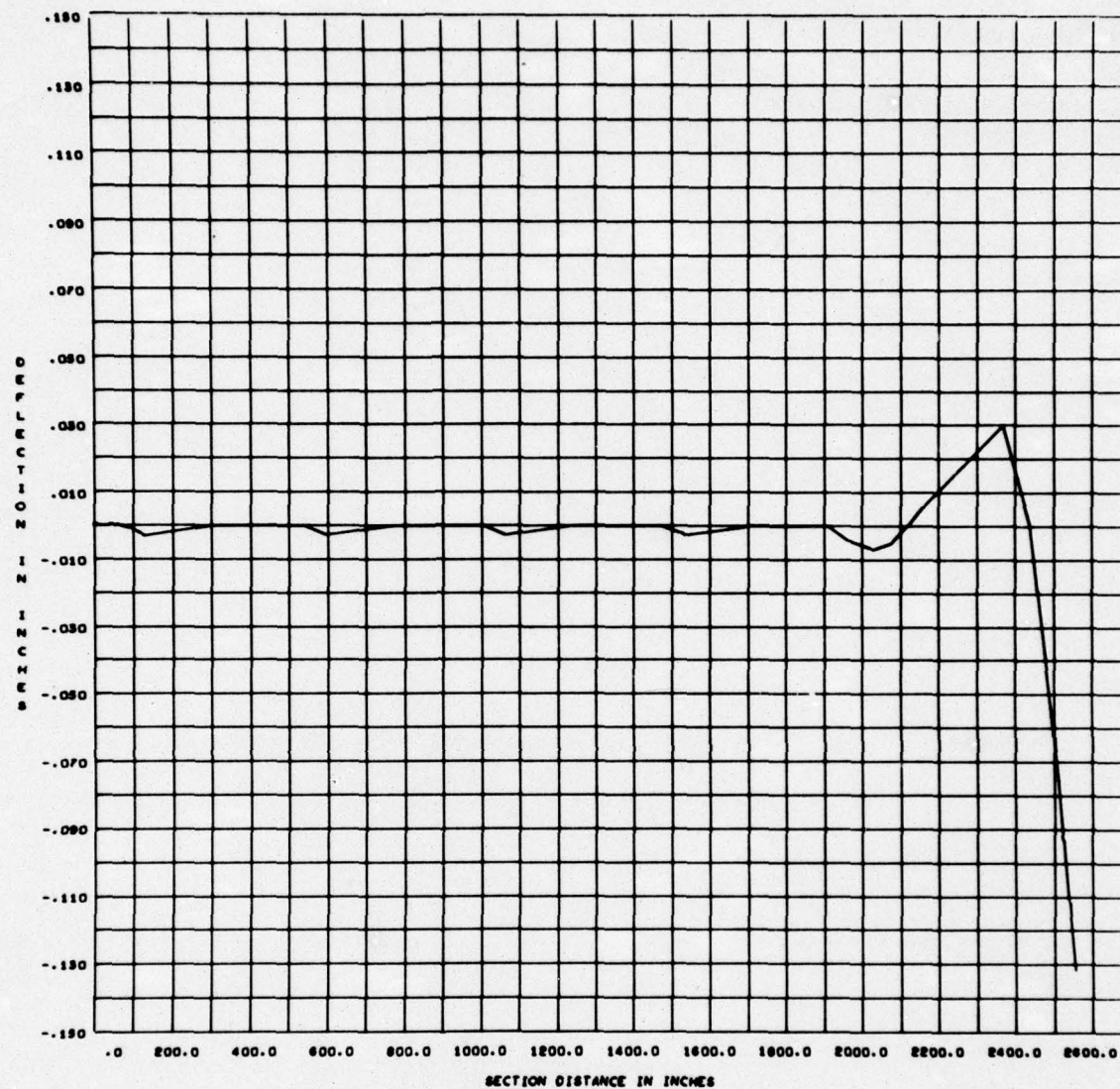
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SAMPLE CASE 12 BEARING SHAFT 1/1/63 1

STATION NO.	SECTION DISTANCE (INCH)	SHAFTING WEIGHT AND STIFFNESS FACTORS			CONCENTRATED WEIGHT OR REACTION (LB.)	BEARING POSITION
		WEIGHT (LB/IN.)	STIFFNESS (1/EI) (X0.000000000001)			
1	0.	-14.2528	165.766400		-0.	-0
2	2.0000	-14.2528	165.766400		-0.	-0
3	4.0000	-72.1547	6.468727		-0.	-0
4	12.5000	-72.1547	6.468727		11222.64	1
5	24.0000	-288.6187	0.404295		-0.	-0
6	40.5000	-288.6187	0.404295		-23160.00	-0
7	57.2500	-72.1547	6.468727		-0.	-0
8	68.5000	-72.1547	6.468727		33679.75	1
9	93.5000	-242.5199	0.572602		-0.	-0
10	98.5000	-72.1547	6.468727		-0.	-0
11	109.5000	-68.2018	7.246302		-0.	-0
12	122.7500	-214.0144	0.735296		-0.	-0
13	130.2500	-64.3602	8.130423		-0.	-0
14	308.5000	-64.3602	8.130423		15285.74	1
15	540.5000	-64.3602	8.130423		15996.47	1
16	590.7500	-214.0144	0.735296		-0.	-0
17	598.2500	-64.3602	8.130423		-0.	-0
18	774.5000	-64.3602	8.130423		15239.26	1
19	1008.5000	-64.3602	8.130423		15997.29	1
20	1058.7500	-214.0144	0.735296		-0.	-0
21	1066.2500	-64.3602	8.130423		-0.	-0
22	1242.5000	-64.3602	8.130423		15278.81	1
23	1476.5000	-64.3602	8.130423		15845.60	1
24	1526.7500	-214.0144	0.735296		-0.	-0
25	1534.2500	-64.3602	8.130423		-0.	-0
26	1698.5000	-64.3602	8.130423		13439.61	1
27	1914.5000	-64.3602	8.130423		23299.63	1
28	1968.5000	-257.4408	0.508151		-0.	-0
29	2028.5000	-74.0893	4.636726		-0.	-0
30	2082.5000	-94.3380	3.542795		-0.	-0
31	2121.5000	-94.3380	3.542795		15898.34	1
32	2160.5000	-90.2282	3.823523		-0.	-0
33	2371.0000	-94.3380	3.542795		-0.	-0
34	2443.0000	-94.3380	3.542795		59460.61	1
35	2515.0000	-74.0893	4.636726		-0.	-0
36	2543.5000	-74.0893	4.636726		-24343.00	-0
37	2559.5000	-49.5618	10.361650		-0.	-0
38	2571.5000	-0.	0.		-0.	-0

A. 36

TOTAL SHAFT WEIGHT (INCLUDING CONCENTRATED LOADS) = -806622.06 LB.  
 DISTANCE OF CENTER OF GRAVITY FROM STATION NO. 1 = 1326.7418 INCH

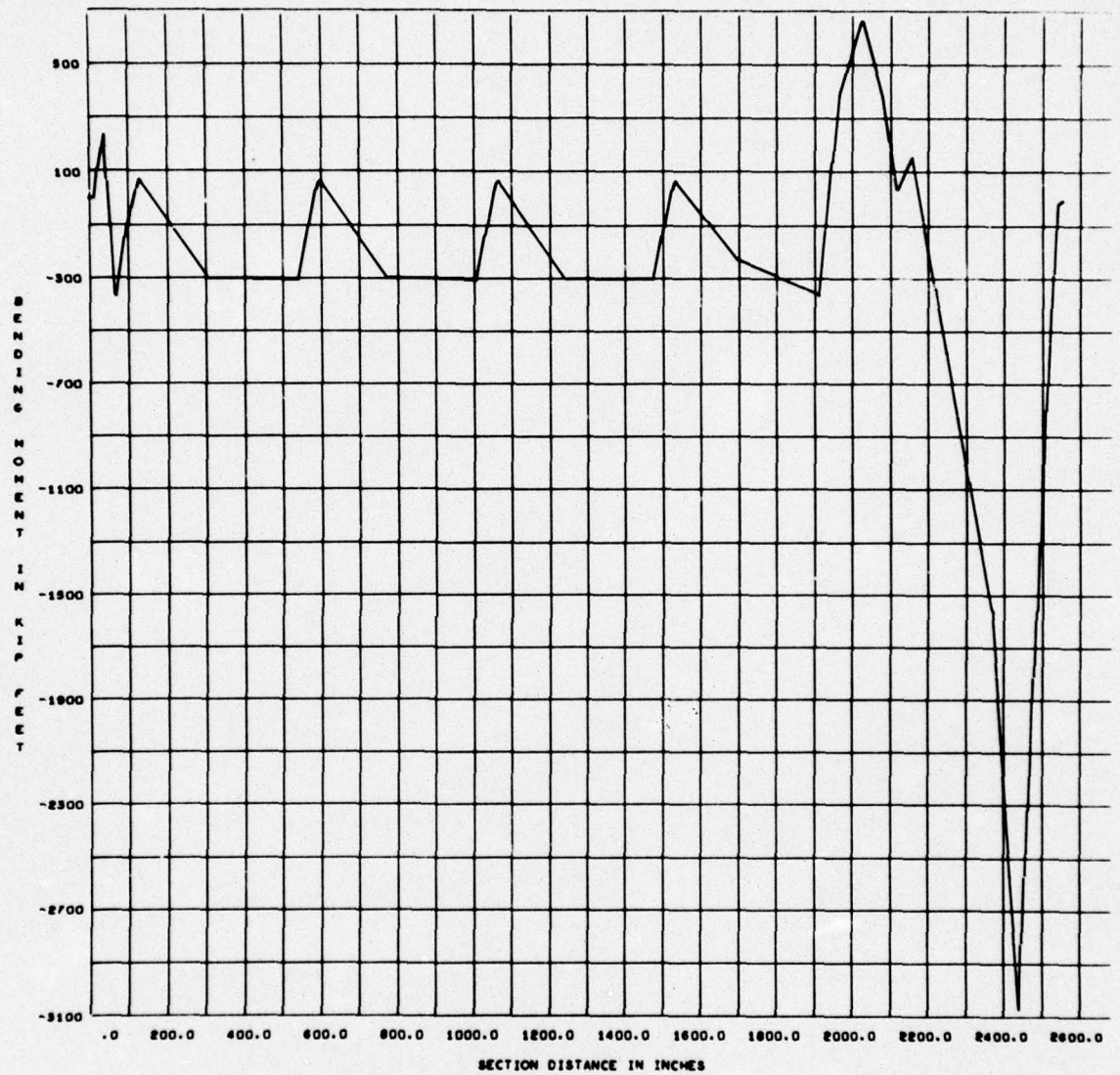


SAMPLE CASE 12 BEARING SHFT 1/1/83

1

Figure A.1 - Sample Graphic Output





SAMPLE CASE 12 BEARING SHAFT 1/1/83

1

Figure A.2 - Sample Graphic Output

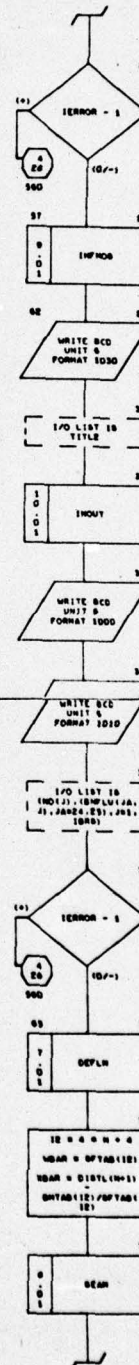
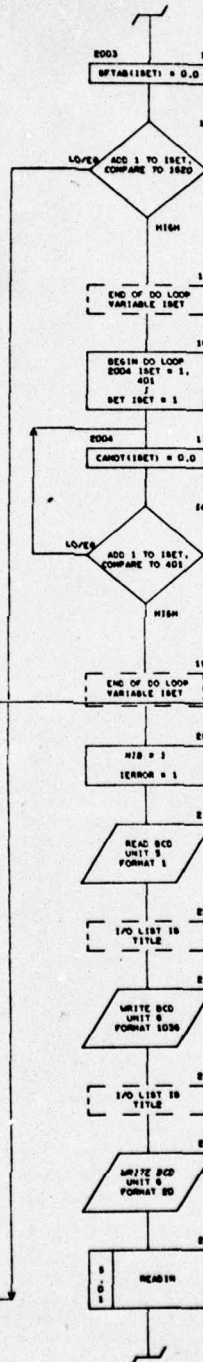
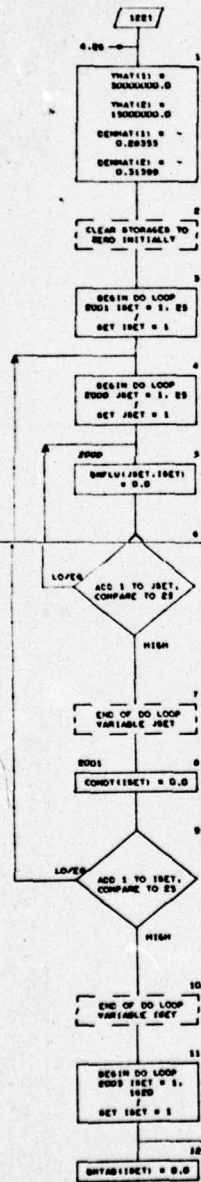
# FLOW CHART

BEST AVAILABLE COPY

DECEMBER

PAGE 1

SHAFTING BEARING  
RECTIONS WHEEL  
S. GOOD CAVIC TAYLOR  
WHEEL GEAR MATERIALS  
STRAIGHT LINE BEARINGS  
RECTIONS  
IDENTIFY MATERIALS  
...STEEL...  
BRONZE...  
RARE...  
WATER...  
DENSITY AND MODULUS FOR  
STEEL, BRONZE

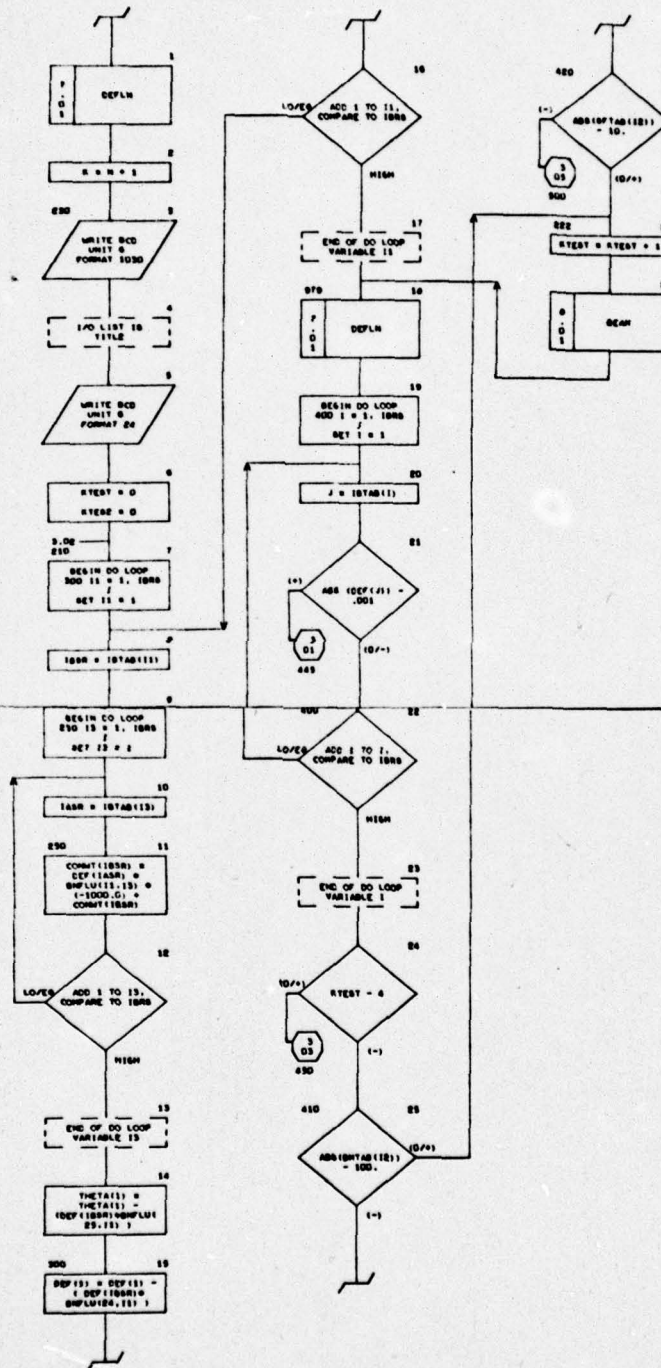




# BEST AVAILABLE COPY

DECR 1002

PAGE 2



PAGE 1





PAGE 4



**BEST AVAILABLE COPY**

### SUBROUTINE READING

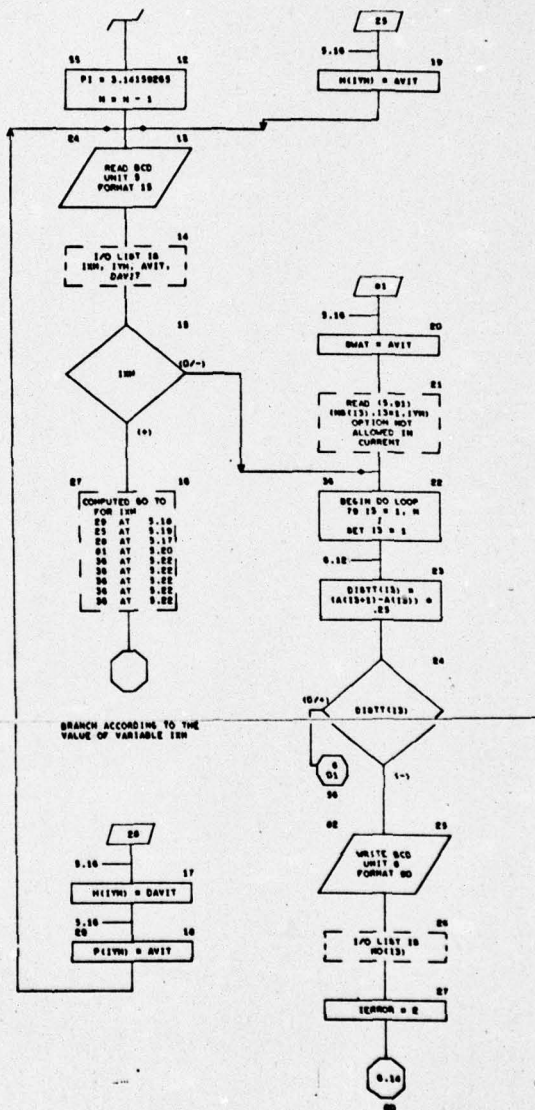
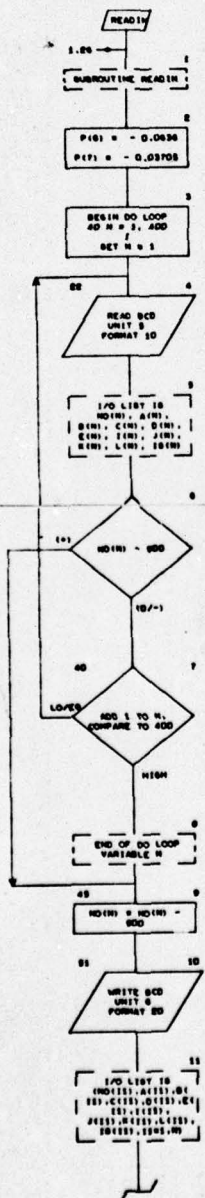
DECK ABOVE

PAGE 9

```

READIN MAGE
NEXT FOR 12TH SENTINEL
BLANK .0 SINGLE CASE
LAST CASE - NO PLOT
12N - 1 NEW DENSITY
2 NEW MODULUS
3 NEW DENSITY AND MODULUS
4 MULTIPLE WY RUN - SPEC
CASE
5.0 NAME AB .0
1 PLOT SINGLE CASE
6 PLOT THEN MULTIPLE
CASES
9 MULTIPLE CASES -
ANOTHER FOLLOW - NO PLOT
WAS NAME USED IN
READING DO NOT MATCH REST
OF PROGRAM

```



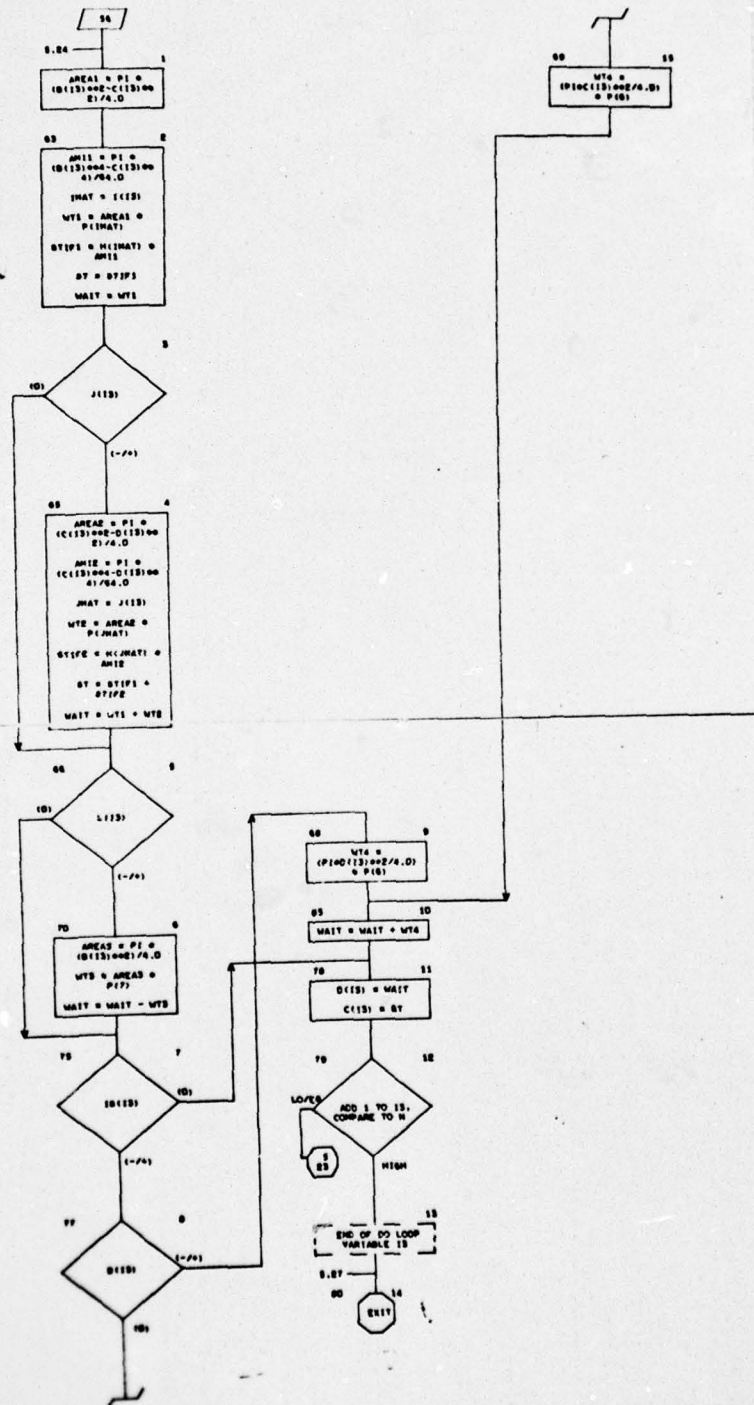


# BEST AVAILABLE COPY

SUBROUTINE READIN

DECK HERE

PAGE 4

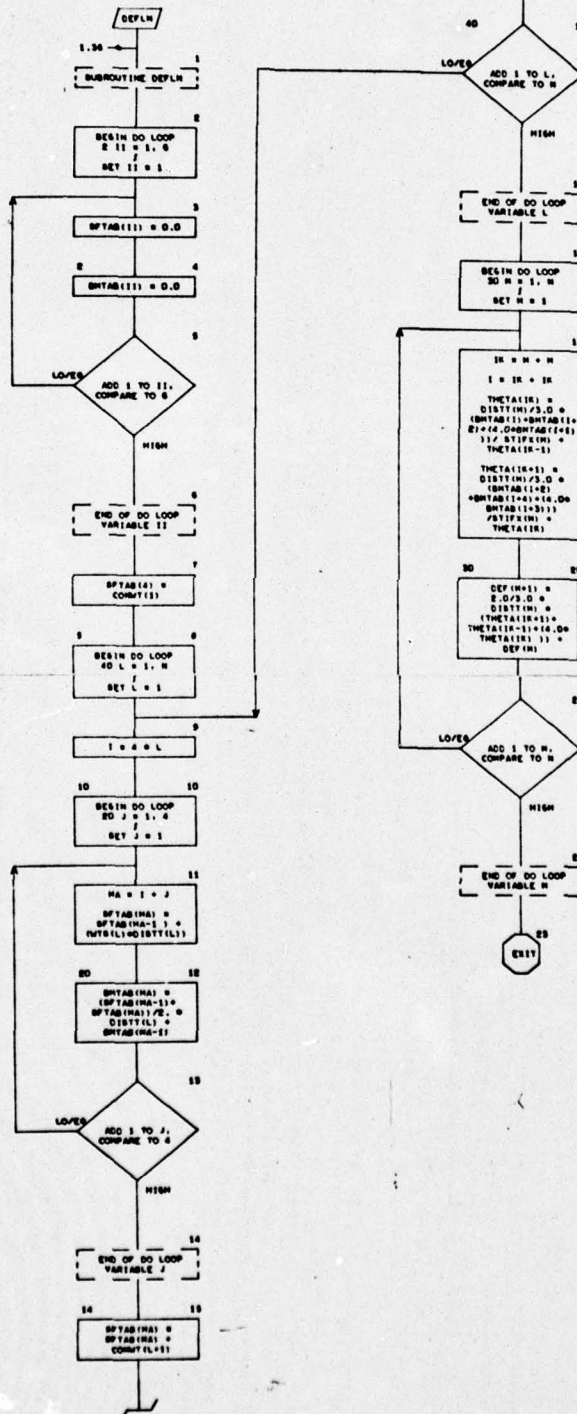


SUBROUTINE DEFLN

DECK DEFL

PAGE 1

DEFLECTION FOR HSES, HSES

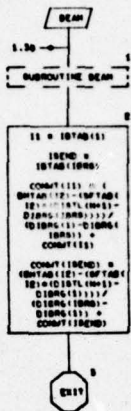




BEST AVAILABLE COPY

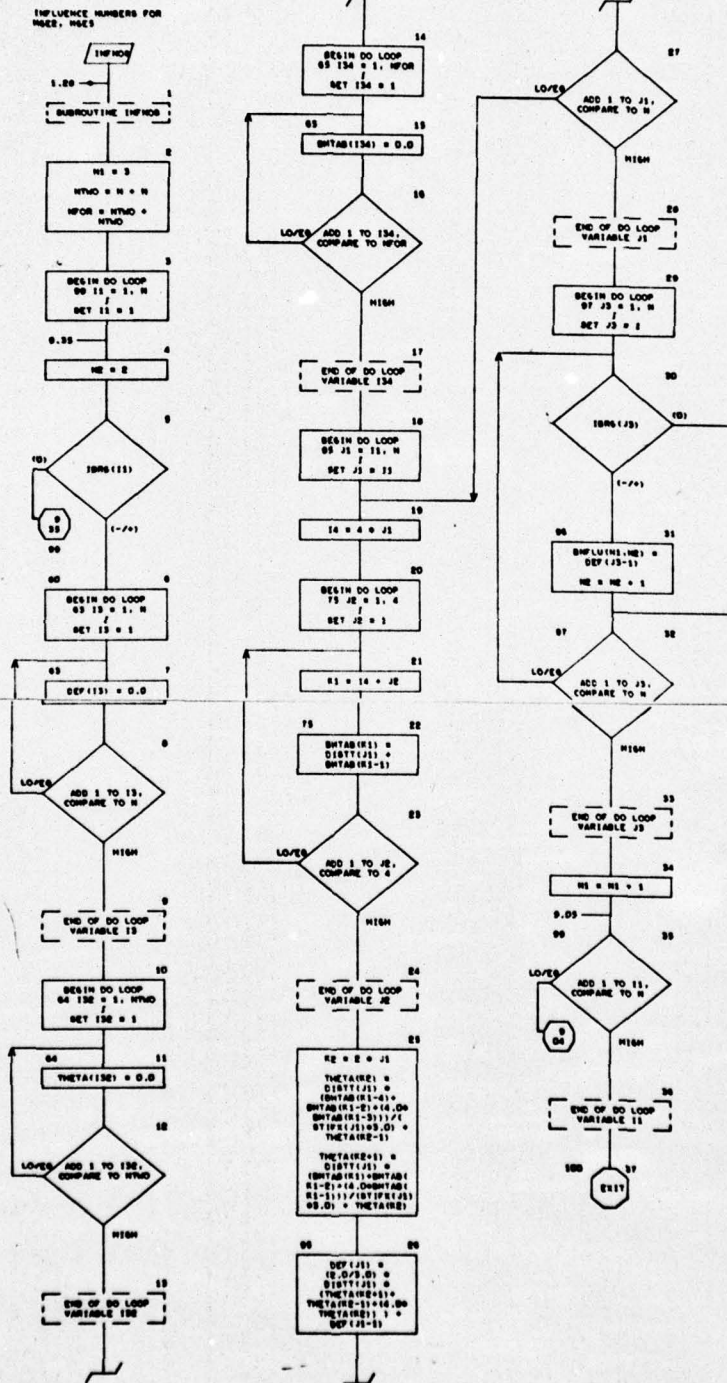
DECE DEANE

PAGE 6



DECR 10074

PAGE 9

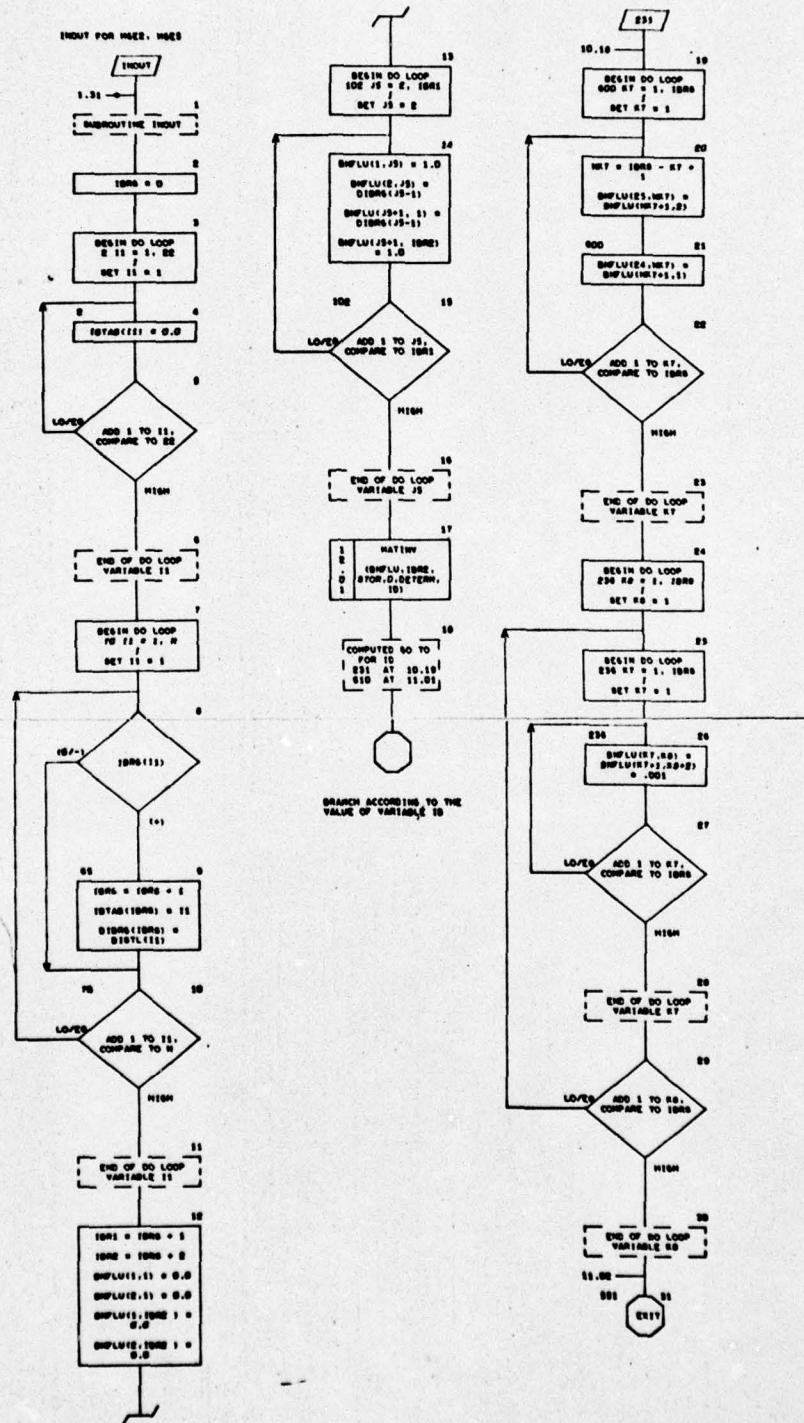




SUBROUTINE INOUT

DECK INOUT

PAGE 10



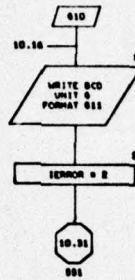
BEST AVAILABLE COPY

SUBROUTINE INOUT

DECK INOUT

PAGE 55

ERROR SET FOR SINGULAR  
ARRAY



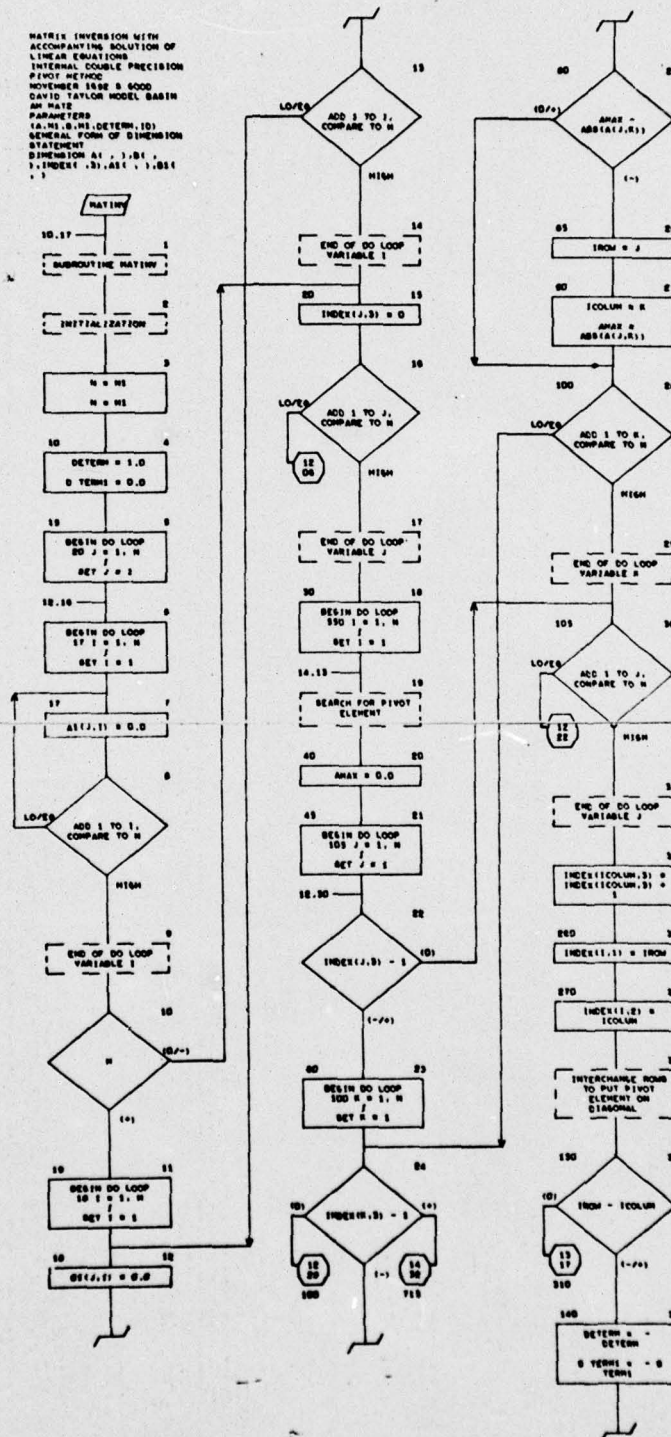


SUBROUTINE MATINV

DECK MATB

PAGE 18

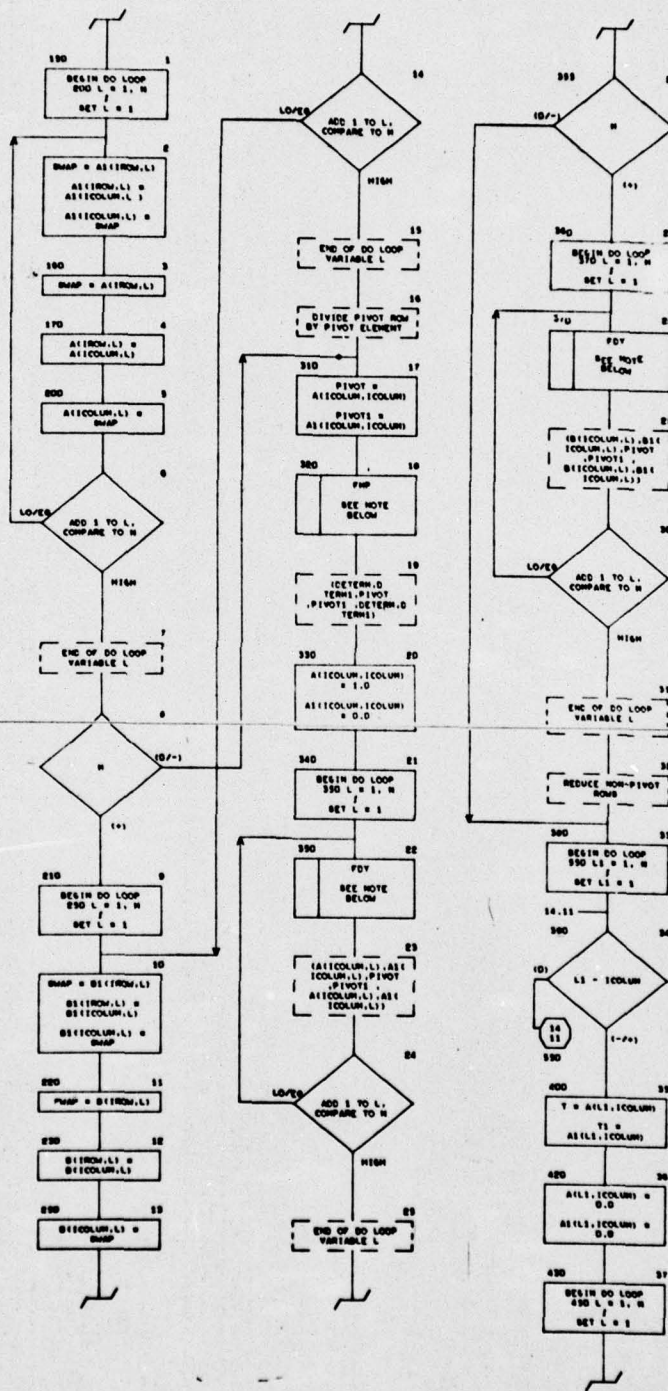
MATRIX INVERSION WITH  
ACCOMPANYING SOLUTION OF  
LINEAR EQUATIONS  
INTERNAL DOUBLE PRECISION  
PIVOT METHOD  
NOVEMBER 1958 S. SODD  
DAVID TAYLOR MODEL BASTIN  
ON HATE  
PARAMETERS  
10. NO. OF ROWS, DETERM. (D)  
GENERAL FORM OF DIMENSION  
STATEMENT  
DIMENSION A(1,1), A(1,1), B(1,1)  
1. INVENT. (3), A(1,1), B(1,1)  
1



SUBROUTINE MATINV

DECR MATB

PAGE 13

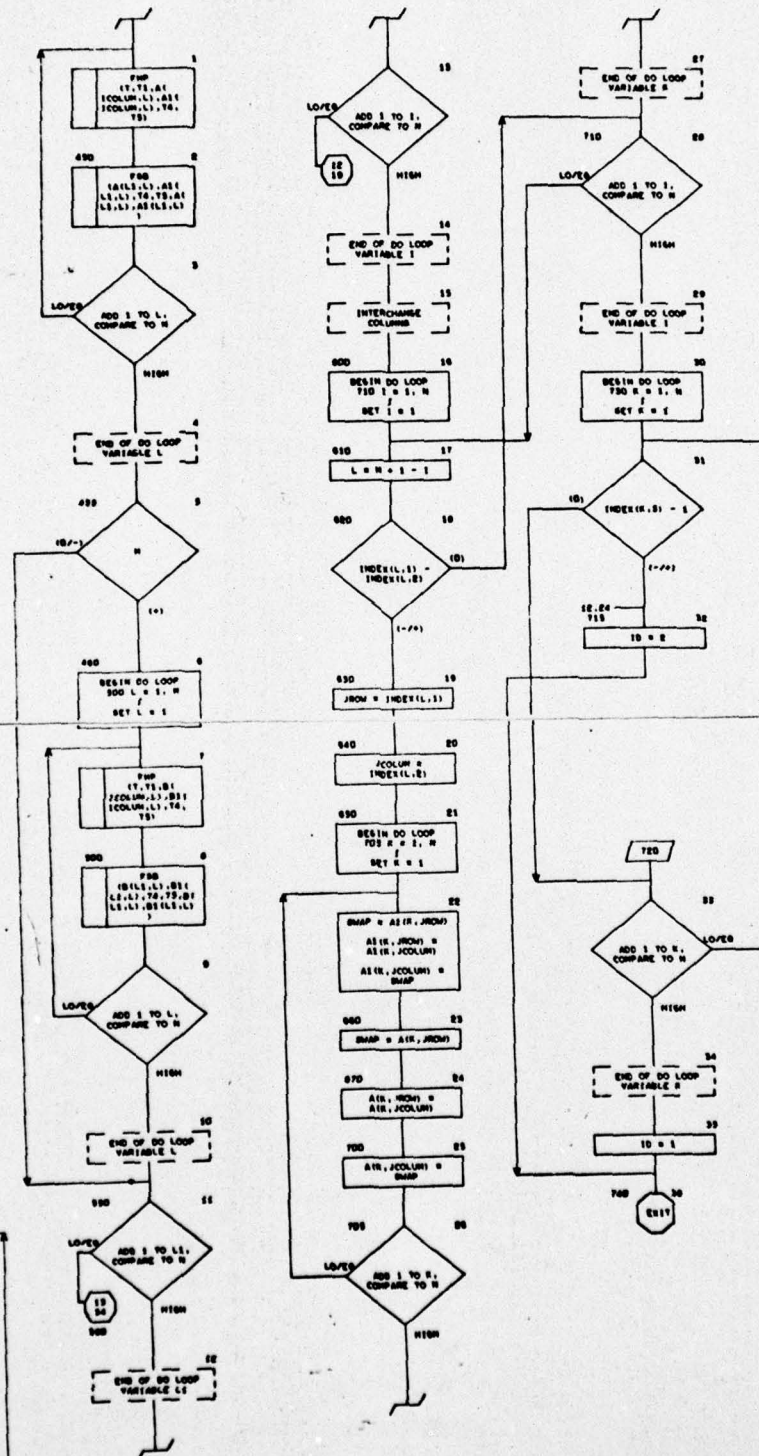




SUBROUTINE MATRIN

DECK MATB

PAGE 14



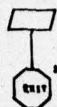
BEST AVAILABLE COPY

SUBROUTINE NAME

DECK NAME

PAGE 10

LAST CARD OF PROGRAM

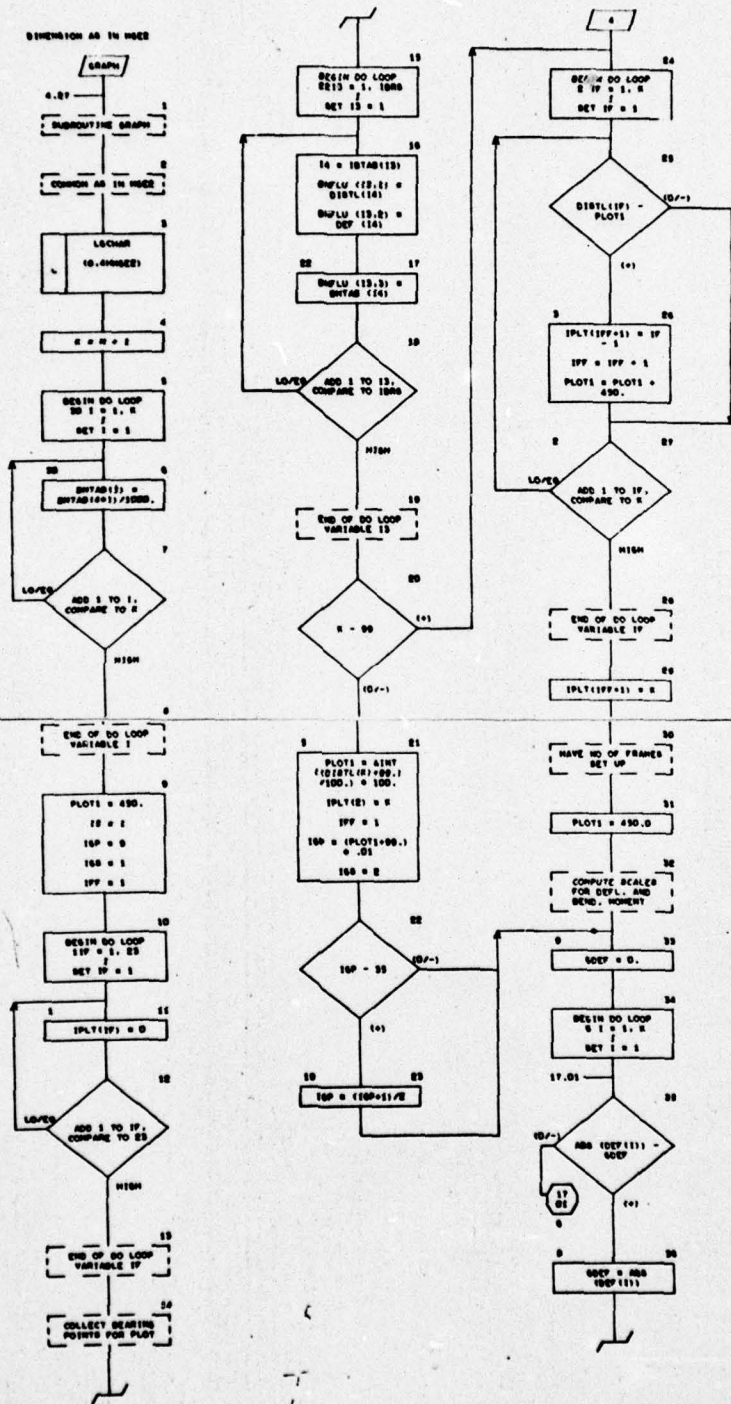




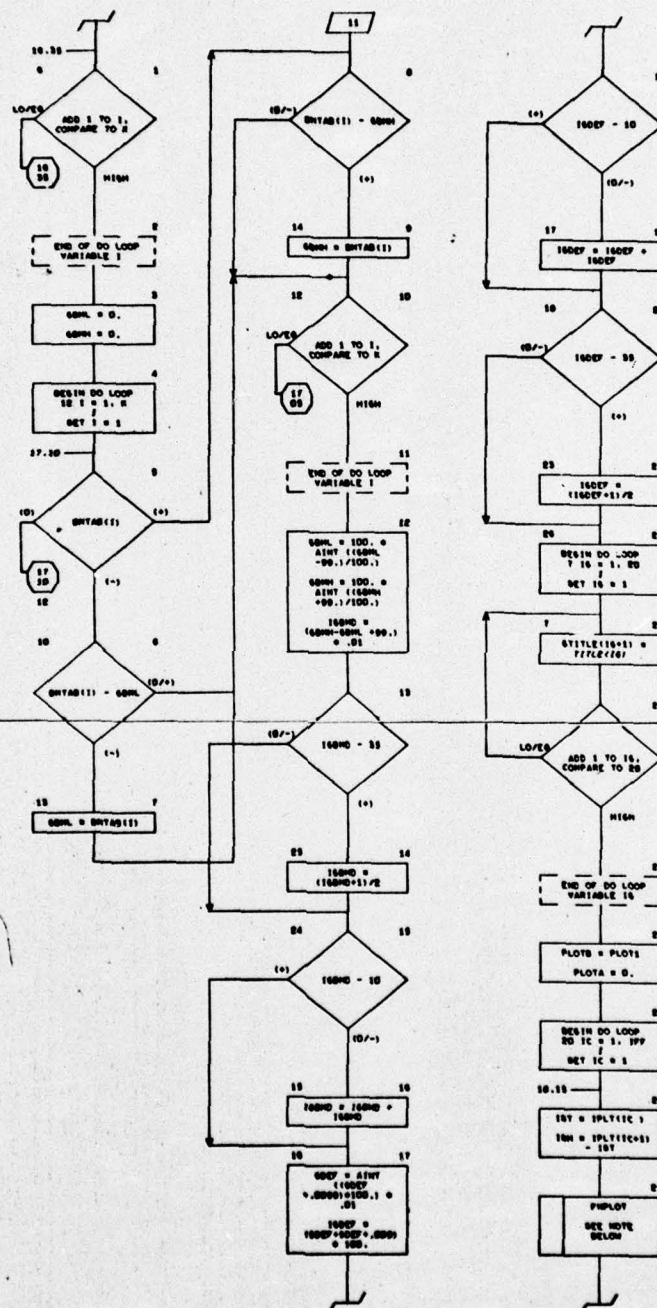
SUBROUTINE GRAPH

DECR GRAPH

PAGE 16



### SUBROUTINE GRAPH

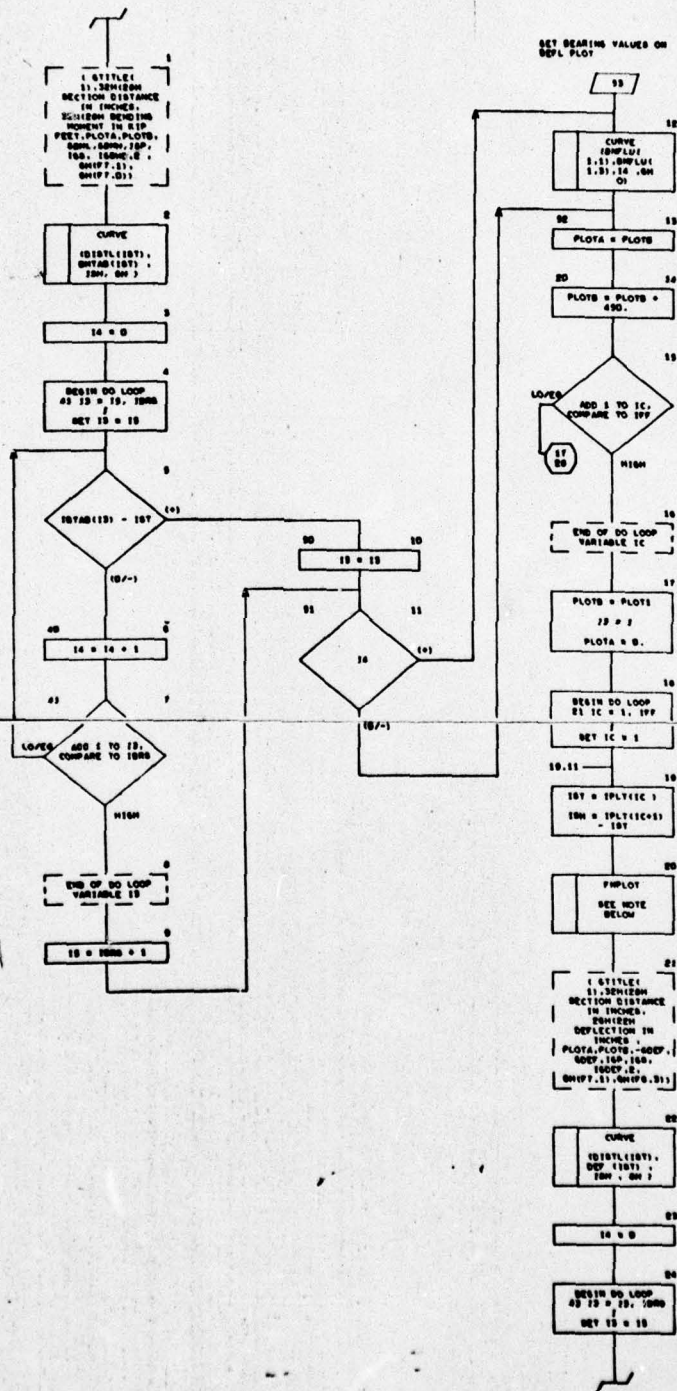




SUBROUTINE GRAPH

DECK GRAPH

PAGE 10

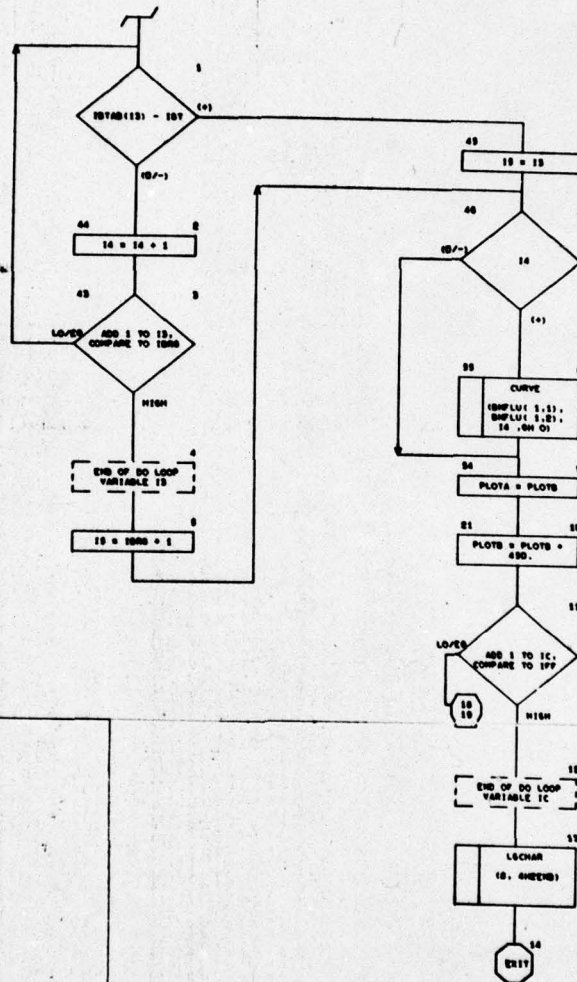


# BEST AVAILABLE COPY

SUBROUTINE GRAPH

DECK GRAPH

PAGE 50





AD-A041 797

NAVAL SHIP RESEARCH AND DEVELOPMENT CENTER BETHESDA --ETC F/G 13/10  
SHIP PROPULSION SHAFTING BEARING REACTION PROGRAMS MGE2 AND MGE--ETC(U)  
AUG 67 S E 600D  
AML-70-67

UNCLASSIFIED

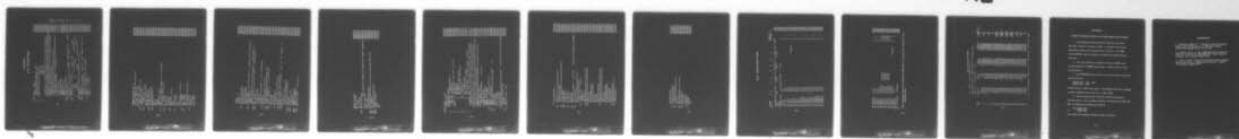
2 OF 2  
ADA  
041797



END

DATE  
FILMED  
8-77

NL



APPENDIX B

MGES - PROGRAM LISTING

```

$IBFTC MGE5 DECK
C SHAFTING BEARING REACTIONS MGE5
C BEARINGS NOT ON STRAIGHT LINE
C IDENTIFY MATERIALS ...STEEL...1
C BRONZE...2
C SAND...6
C WATER...7
C
C DIMENSION DISTL(401),DIAL(401),STIFX(401),WTS(401),CONWT(401),
1 IM(401),JM(401),IBRG(401),IWATR(401),IS(401),YMAT(7),DENMAT(7),
2 DISTT(401), RMTAB(1620),THETA(802),DEF(401),BNFLU(25),DIBRG(25)
3,IBTAB(25), SFTAB(1620),TITL2(12),TITL5(12),XBRG(25),NO(400)
C DIMENSION CANOT(401),CONOT(25)
C COMMON N,NO,DISTL,DIA,STIFX,WTS,CONWT,IM,JM,IBRG,
1 IWATR,IS,YMAT,DENMAT,DISTT,BMTAB,THETA,DEF,BNFLU,DIBRG,IBTAB,
2 IBRS,SFTAB,I2,IERROR, TITL2,IXM
C DIMENSION NS(50)
C COMMON SWAT,NS,IYM
C COMMON TITL5,XBRG
1 FORMAT(12A6)
2 FORMAT(11, 5F11.8)
1030 FORMAT(1H120X,12A6///)
1032 FORMAT(110H0
1R RAISED FROM ORIGINAL STRAIGHT LINE DATUM
1037 FORMAT(F14.1,10F10.1)
1040 FORMAT(110H STATION SHEAR FORCE BEARING / MOMENT
1 SLOPE DEFLECTION (KIP.) REACTION (LBS.)
2 113H NO. (INCH)
1 (RADIANS)
1050 FORMAT(I9,-3PF21.5,F19.3,OPF20.7,F20.7,F16.1)
1097 FORMAT(11)
1036 FORMAT(1H1 20X 45H *** SHAFTING SYSTEM PROGRAM MGE5 ***
1////20X,12A6/20X12A6)
C DENSITY AND MODULUS FOR STEEL, BRONZE
1221 YMAT(1)=30000000.0
YMAT(2)= 15000000.0
DENMAT(1)=-0.28355

```



MGE50037  
 MGE50038  
 MGE50039  
 MGE50040  
 MGE50041  
 MGE50042  
 MGE50043  
 MGE50044  
 MGE50045  
 MGE50046  
 MGE50047  
 MGE50048  
 MGE50049  
 MGE50050  
 MGE50051  
 MGE50052  
 MGE50053  
 MGE50054  
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 MGE50058  
 MGE50059  
 MGE50060  
 MGE50061  
 MGE50062  
 MGE50063  
 MGE50064  
 MGE50065  
 MGE50066  
 MGE50067  
 MGE50068  
 MGE50069  
 MGE50070  
 MGE50071  
 MGE50072

```

C
DENMAT(2)=-0.31399
CLEAR STORAGES TO ZERO INITIALLY
DO 2001 ISET=1,25
DO 2000 JSET = 1,25
  BNFLU(JSET,ISET) = 0.0
  XBRG(ISET) = 0.0
  CONOT(ISET) = 0.0
DO 2003 ISET=1,1620
  BMTAB(ISET)=0.0
  SFTAB(ISET)=0.0
DO 2004 ISET=1,401
  CANOT(ISET)=0.0
  N76 =5
  N77=1
  IERROR = 1
  READ (5,1) TITL5
231  READ (5,2) IMOVE, (XBRG(I77),I77=N77,N76)
  IF (IMOVE) 220,230,220
230  N76 =N76+5
  N77=N77+5
  GO TO 231
220  CONTINUE
  READ (5,1) TITL2
  NIB=1
50  CALL READIN
  IXM = IXM
  N=N
  IF(IERROR-1) 57,57,560
57  CALL INFNOS
63  CALL INOUT
  IBRS = IBRS
  IF(IERROR-1) 65,65,560
65  CALL DEFLN
  I2=4*N+4
  CALL BEAM
  CALL DEFLN

```

MGE50073  
 MGE50074  
 MGE50075  
 MGE50076  
 MGE50077  
 MGE50078  
 MGE50079  
 MGE50080  
 MGE50081  
 MGE50082  
 MGE50083  
 MGE50084  
 MGE50085  
 MGE50086  
 MGE50087  
 MGE50088  
 MGE50089  
 MGE50090  
 MGE50091  
 MGE50092  
 MGE50093  
 MGE50094  
 MGE50095  
 MGE50096  
 MGE50097  
 MGE50098  
 MGE50099  
 MGE50100  
 MGE50101  
 MGE50102  
 MGE50103  
 MGE50104  
 MGE50105  
 MGE50106  
 MGE50107  
 MGE50108

```

K=N+1
KTEST = 0
KTES2=0
210 DO 300 I1=1,IBRS
    IBSR=IBTAB(I1)
    DO 250 I3=1,IBRS
        IASR=IBTAB(I3)
        250 CONWT(IBSR) = (DEF(IASR)-XBRG(I3 ))*BNFLU(I1,I3)*(-1000.0)+
            1 CONWT(IBSR)
        THETA(I1)= THETA(I1)-((DEF(IBSR)-XBRG(I1 ))*BNFLU(25,I1) )
        300 DEF(I1) =DEF(I1)-((DEF(IBSR)- XBRG(I1 ))*BNFLU(24,I1) )
        979 CALL DEFLN
        DO 400 I=1,IBRS
            J=IBTAB(I)
            IF(ABS (DEF(J)-XBRG(I))-0.001) 400,400,445
            400 CONTINUE
            IF(KTEST-4) 410, 450, 450
            410 IF(ABS (BMTAB(I2))-100.)420,222 ,222
            420 IF(ABS (SFTAB(I2))- 10.)500,222,222
            222 KTEST = KTEST +1
            CALL BEAM
            GO TO 979
            445 KTES2=KTES2+1
            IF (KTES2-4) 210, 450, 450
            450 WRITE (6,451) KTES2, KTEST
            451 FORMAT(27H0100 MANY ITERATIONS - DEFL I4, 9H MOMENT I4)
            500 DO 515 I=1,K
                DIST(I)= 0.0
                IF (STIFX(I))515,515,514
            514 DIST(I)=1.E12/STIFX(I)
            515 CONTINUE
            800 DO 825 I=1,IBRS
                J=IBTAB(I)
                820 CONOT(I)=CONWT(J)
                825 CANOT(J)=CONOT(I)
            540 WRITE (6,1036) I,I1L5,I1I1L2
  
```



```

WRITE (6,1040)
DO 545 I=1,K
  IB = I+1
  IA = IB+IB
545 WRITE (6,1050)
      1 NO(I),SFTAB(IA),BMTAB(IA),THETA(IB-1),DEF(I),CANOT(I)
      WRITE (6,1032)
      IXM = IXM
      IF(IXM)1222,1222,980
980 GO TO(1222,1222,1222,1222,1222,1222,981,981,1221),IXM
981 CALL GRAPH
560 IF(IXM-7)1222,1222,1221
1222 WRITE (6,1036)
      STOP
      END

```

B. 4

```

MGE50109
MGE50110
MGE50111
MGE50112
MGE50113
MGE50114
MGE50115
MGE50116
MGE50117
MGE50118
MGE50119
MGE50120
MGE50121
MGE50122
MGE50123

```

```

$IBFTC RED5 DECK
C READIN MGE5
SUBROUTINE READIN
SECOND CASE BEARING RAISED
KEY FOR IXM SENTINEL
BLANK #0 SINGLE CASE, LAST CASE - NO PLOT
IXM - 1 NEW DENSITY
2 NEW DENSITY
3 NEW DENSITY AND MODULUS
4 MULTIPLE WT RUN - SPEC CASE
5,6 SAME AS #0
7 PLOT SINGLE CASE
8 PLOT THEN MULTIPLE CASES
9 MULTIPLE CASES - ANOTHER FOLLOWS - NO PLOT
C VARIABLE NAMES USED IN READIN DO NOT MATCH REST OF PROGRAM
DIMENSION A(401), B(401), C(401), D(401), E(401), I(401), J(401),
1K(401), L(401), IS(401), H( 7), P( 7), DISTT(401), BMTAB(1620),
2THETA(802), DEF(401), BNFLU(25,25), DIBRG(25), IBTAB(25), SFTAB(1620),
3TITL2(12), TITL5(12), XBRG(25), NO(400)
COMMON N,NO,A,B,C,D,E,I,J,K,L,IS,H,P,DISTT,BMTAB,THETA,DEF,
IBNFLU,DIBRG,IBTAB,
2 IBRS,SFTAB,I2,IERROR, TITL2,IXM
DIMENSION NS(50)
COMMON SWAT,NS,IYM
COMMON TITL5,XBRG
10 FORMAT( I3,5F12.4,2I2,3I1)
15 FORMAT (2I2,2F12.2)
90 FORMAT(25H0 STATION DISTANCE ERROR I5)
91 FORMAT(24I3)
P(6)=-0.0636
P(7)=-0.03705
DO 40 N=1,400
22 READ(5,10)NO(N),A(N),B(N),C(N),D(N),E(N),I(N),J(N),K(N),L(N),IS(N)
IF(NO(N)-900)40,40,45
40 CONTINUE
45 NO(N) = NO(N) -900

```

RED50002  
 RED50003  
 RED50004  
 RED50005  
 RED50006  
 RED50007  
 RED50008  
 RED50009  
 RED50010  
 RED50011  
 RED50012  
 RED50013  
 RED50014  
 RED50015  
 RED50016  
 RED50017  
 RED50018  
 RED50019  
 RED50020  
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 RED50071  
 RED50072  
 RED50073

```

55 PI=3.14159265
   N = N-1
24 READ (5,15) IXM,IYM,AVIT,DAVIT
   IF (IXM) 36,36,27
27 GO TO (29,25,28,81,36,36,36,36),IXM
28 H(IYM)=DAVIT
29 P(IYM)=AVIT
   GO TO 24
25 H(IYM)=AVIT
   GO TO 24
81 SWAT=AVIT
C READ (5,91) (NS(II), II=1,IYM)
36 DO 79 I3=1,N
   DISTT(I3)=(A(I3+1)-A(I3))*25
   IF (DISTT(I3))82,56,56
82 WRITE (6,90) NO(I3)
   IERROR = 2
   GO TO 80
56 AREA1=PI*(B(I3)**2-C(I3)**2)/4.0
63 AMI1=PI*(B(I3)**4-C(I3)**4)/64.0
   IMAT=I(I3)
   WT1=AREA1*P(IMAT)
   STIF1=H(IMAT)*AMI1
   ST=STIF1
   WAIT=WT1
   IF (J(I3))65,66,65
65 AREA2=PI*(C(I3)**2-D(I3)**2)/4.0
   AMI2=PI*(C(I3)**4-D(I3)**4)/64.0
   JMAT=J(I3)
   WT2=AREA2*P(JMAT)
   STIF2=H(JMAT)*AMI2
   ST=STIF1+STIF2
   WAIT=WT1+WT2
66 IF (L(I3))70,75,70
70 AREA3=PI*(B(I3)**2)/4.0
   WT3=AREA3*P(7)
  
```

OPTION NOT ALLOWED IN CURRENT

```

WAIT=WAIT-WT3
75 IF(I3(I3))77,78,77
77 IF(D(I3))68,69,68
69 WT4=(PI*C(I3)**2/4.0)*P(6)
GO TO 85
68 WT4=(PI*D(I3)**2/4.0)*P(6)
85 WAIT=WAIT+WT4
78 D(I3)=WAIT
C(I3)=ST
79 CONTINUE
80 RETURN
END

```

B.7

```

RED50074
RED50075
RED50076
RED50077
RED50078
RED50079
RED50080
RED50081
RED50082
RED50083
RED50084
RED50085

```



[illegible]

**B. 8**





# MGES - SAMPLE OUTPUT SHEET

\*\*\* SHAFTING SYSTEM PROGRAM MGES \*\*\*

RAISING BRGS 3.4.5.6 TO EQUALIZE OPERATING L.S. GEAR BRG. LOADS

SAMPLE CASE 12 BEARING SHAFT 4/1/64

STATION NO.	SHEAR FORCE (KIP.)	MOMENT (KIP.-INCH)	SLOPE (RADIANS)	DEFLECTION (INCH)	BEARING REACTION (LBS.)
1	-0.	0.	-0.0000114	0.0201429	0.
2	-0.02851	-0.029	-0.0000114	0.0201201	0.
3	-0.05701	-0.114	-0.0000114	0.0200973	0.
4	19.95398	-3.205	-0.0000118	0.0200000	20624.3
5	19.12420	221.494	-0.0000038	0.0199989	0.
6	-8.73801	497.755	-0.0000009	0.0198618	0.
7	-13.57237	310.906	0.0000019	0.0199729	0.
8	6.79524	153.651	0.0000189	0.0200000	21179.4
9	4.99137	300.983	0.0000562	0.0200893	0.
10	3.77877	322.909	0.0000371	0.0211727	0.
11	2.98507	360.110	0.0000018	0.0219327	0.
12	2.08139	393.675	0.0001177	0.0233491	0.
13	0.47629	403.266	0.0001199	0.0231404	0.
14	7.88510	-512.433	0.0002805	0.0208999	10762.2
15	8.83585	-429.372	-0.0000507	0.0181799	16011.0
16	5.60175	-66.628	-0.0001528	0.0939228	0.
17	3.99664	-30.634	-0.0001528	0.0947780	0.
18	7.73249	-325.870	-0.0001694	0.0785983	15099.8
19	8.71686	-278.522	-0.0001856	0.0203957	10004.7
20	5.48276	78.243	-0.0002210	0.0186674	0.
21	3.87765	113.345	-0.0002205	0.0185116	0.
22	6.98398	-202.864	-0.0000459	-0.0000087	14469.8
23	8.46648	-330.665	0.0000063	-0.0000157	16042.8
24	5.23238	13.519	-0.0000339	-0.0018265	0.
25	3.62727	46.742	-0.0000338	-0.0033308	0.
26	6.29193	-225.635	0.0000200	-0.0000253	13895.8
27	15.74768	-367.973	-0.0000618	-0.0000382	23267.8
28	12.27223	308.564	-0.0000504	-0.0045619	0.
29	-3.17422	661.504	-0.0000320	-0.0070765	0.
30	-7.17504	382.074	0.0001031	-0.0048424	0.
31	5.02968	30.504	0.0001341	-0.0000538	15083.9
32	1.35050	154.917	0.0001490	0.0040996	0.
33	-17.64255	-1559.821	-0.0001482	0.0297004	0.
34	35.02703	-3074.609	-0.0007453	-0.0000824	59461.9
35	28.23470	-797.186	-0.0012424	-0.0782218	0.
36	1.78015	-22.587	-0.0012959	-0.1118345	0.
37	0.59473	-3.588	-0.0012967	-0.1323769	0.
38	-0.03002	-0.019	-0.0012969	-0.1479388	0.

\* WITH CERTAIN BEARINGS LOWERED OR RAISED FROM ORIGINAL STRAIGHT LINE DATUM

## APPENDIX C

### NOTES ON MODIFICATION FOR OTHER COMPUTER SYSTEMS

1. A programmed double-precision arithmetic was used internally in matrix inversion on 7090. A computer with greater significance might use a single-precision version, or the LARC version MAT2L might be modified to avoid the assembly language subroutine.

2. Use of SC 4020 option assumes a library of MAP coded routines available on NSRDC system tape. A FAP version of these routines exists.

3. For FORTRAN II use insert F on library and open subroutine names as follows:

MGE2 0104, 0108, 0109  
MAT2 0040, 0037

A FAP version of DPAF also exists. Card MGE2 0159 may be changed to reflect standard system stop; e.g., CALL EXIT.

4. Total allowed number of stations (400) would handle an aircraft carrier. For a smaller computer, all dimensions of 400, 401 802, and 1620 may be reduced equivalently.

Card RED2 0032  
or RED5 0032

must reflect the maximum allowed number of stations.



## REFERENCES

1. Antkowiak, Edward T., "Calculation of Ship Propulsion Shafting Bearing Reactions on an IBM 650 Computer," Boston Naval Shipyard Report R-11 (1967).
2. Anderson, H.C., et. al., "Shafting Systems Programs MGE-402 and MGE-405," DR59MSD-202, General Electric Company, Lynn, Massachusetts (1959).
3. Luvisi, Joseph, "Calculation of Ship Propulsion Shafting Bearing Reactions on a Datatron 205 Computer," Boston Naval Shipyard Report R-24.

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